



# ECS Florida, LLC

Geotechnical Engineering Report

**Titusville Resort and Destination – Post Demolition Phase**

3550 South Washington Avenue  
Titusville, Brevard County, Florida 32780

ECS Project Number 56:1380-B

May 13, 2024 - Revised





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Mr. Jesse Wright, CEO  
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ECS Project No. 56:1380-B

Reference: Geotechnical Engineering Report  
**Titusville Resort & Destination – Post Demolition Phase**  
3550 South Washington Avenue  
Titusville, Brevard County, Florida 32780

Dear Mr. Wright:

ECS Florida, LLC (ECS) has completed the subsurface exploration, laboratory testing, and geotechnical engineering analyses for the above-referenced project (Phases 1 and 2). Our services were performed in general accordance with our agreed-to scope of work. This report presents our understanding of the geotechnical aspects of the project along with the results of the field exploration and laboratory testing conducted, and our foundation design and earthwork construction recommendations. This report includes the remainder of the required seven (7) additional Standard Penetration Test (SPT) borings performed within the razed building footprints, along with a pressure-meter test scope.

It has been our pleasure to be of service to **Titusville Resort and Destination, LLC** during the design phase of this project. We would appreciate the opportunity to remain involved during the construction phase operations as well to verify the assumptions of subsurface conditions made for this report. Please contact us if you have any questions concerning this report, or if we can be of further assistance.

Respectfully submitted,  
**ECS Florida, LLC**

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## TABLE OF CONTENTS

<b>EXECUTIVE SUMMARY .....</b>	<b>1</b>
<b>1.0 INTRODUCTION .....</b>	<b>3</b>
<b>2.0 PROJECT INFORMATION .....</b>	<b>4</b>
2.1 Project Location/Current Site Use.....	4
2.2 Past Site History/Uses .....	4
2.3 Soil Survey Mapping.....	4
2.4 Proposed Construction.....	5
<b>3.0 FIELD EXPLORATION AND LABORATORY TESTING .....</b>	<b>7</b>
3.1 Subsurface Characterization FROM BORINGS.....	7
3.2 pressuremeter testing.....	8
3.3 Groundwater Observations.....	8
Estimated Seasonal High Groundwater.....	8
3.4 Laboratory Testing .....	9
<b>4.0 DESIGN RECOMMENDATIONS.....</b>	<b>10</b>
4.1 Foundation AREA preparation .....	10
4.2 Foundation DESIGN.....	10
4.3 Slabs On Grade.....	11
4.4 Pavements.....	12
4.4.1 Flexible Pavement Recommendations .....	12
4.4.2 Rigid Pavement Recommendations.....	12
4.5 Stormwater Management Facilities.....	13
4.5.1 Soil Permeability Rate.....	13
4.5.2 Borrow Suitability .....	13
4.6 Below Grade Pool Design Recommendations.....	14
4.6.1 General .....	14
4.6.2 Uplift Protection .....	14
<b>5.0 SITE CONSTRUCTION RECOMMENDATIONS.....</b>	<b>15</b>
5.1 Subgrade Preparation .....	15
5.1.1 Stripping and Grubbing.....	15
5.1.2 Proofrolling.....	15
5.1.3 Temporary Groundwater Control.....	15
5.1.4 Subgrade Compaction .....	16
5.2 Earthwork Operations.....	16
5.2.1 Structural Backfill and Fill Soils .....	16
5.2.2 Foundation Areas.....	17
5.2.3 Flexible Pavement Areas.....	17
5.2.4 Rigid Pavement Areas.....	18
5.3 Utility Installations .....	18
<b>6.0 CLOSING.....</b>	<b>20</b>

## **APPENDICES**

### **Appendix A – Drawings & Reports**

- Figure 1 - Site Location Diagram
- Figure 2 – Boring Location Diagram

### **Appendix B – Field Operations**

- Reference Notes for Boring Logs
- Subsurface Exploration Procedure: Standard Penetration Testing (SPT) ASTM D1586
- Subsurface Exploration Procedure: Hand Auger Borings ASTM D1452
- SPT Boring Logs
- Auger Boring Logs

### **Appendix C – Laboratory Test Results**

- Laboratory Test Results Summary

### **Appendix D – Pressuremeter Test Results**

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## EXECUTIVE SUMMARY

This Executive Summary is intended as a very brief overview of the primary geotechnical conditions that are expected to affect design and construction of the proposed Titusville Resort and Destination project, Phases 1 and 2, to be located at 3550 South Washington Avenue in Titusville, Brevard County, Florida. The project will include design and construction of one 4-story assisted living building and one 6-story multifamily residential building with an observation deck, along with a leasing/club house building and swimming pool, a 5-story hotel building with attached 1-story restaurant building and multiple 1-story commercial buildings with associated paved parking, drive areas and stormwater areas, rain garden and bioswales. Information gleaned from the Executive Summary should not be utilized in lieu of reading the entire geotechnical report.

- Based on the results of our exploration borings and pressuremeter testing, we consider the subsurface conditions at the site adaptable for support of the proposed structures on a properly designed conventional shallow foundation system with a maximum allowable bearing pressure of up to 5,000 psf. Provided the site preparation and earthwork construction recommendations outlined in Section 5.0 of this report are performed, the parameters presented in Section 4.1 of this report may be used for foundation design.
- We consider the subsurface conditions at the site favorable for support of flexible and rigid pavement sections when constructed on properly prepared subgrade soils as outlined in Section 5.0 of this report.
- Very loose to loose soils sands were encountered in the upper 2 to 10 feet below the existing ground surface at some of the boring locations. As outlined in Section 5.1.4, a heavy vibratory roller should be used to compact the surface soils below the proposed footings. To further compact the soil below the proposed hotel footprint, we recommend over-excavating the upper 3 feet of soil within foundation areas before compaction of the subgrade with the heavy vibratory roller. Dynamic cone penetrometer (DCP) soundings should also be performed subsequent to the surface soil heavy compaction operations to confirm densification of the sands as recommended herein. This recommendation is particularly important due to the higher allowable bearing pressure provided herein as a result of the pressuremeter testing performed by ECS.
- The fine sand (SP), fine sand with clay (SP-SC) and fine sand with silt (SP-SM) encountered at the stormwater management area boring locations from existing ground surface to depths of 10 feet below ground surface may be used as structural fill soil.
- The borings encountered groundwater at depths varying from 4.5 to 6 feet below the existing ground surface at the time of our exploration, and the normal seasonal high groundwater level is estimated to be up to 1-foot higher than the levels estimated at the time of drilling. Groundwater control may be necessary in order to compact the existing soils and install shallow foundations. Temporary groundwater control measures will be required for deeper excavations, such as those typically required to install utilities.

- Boring locations PB-03 through PB-05 are considered preliminary for Phase 3, including Buildings A, B, C, and D, as shown on the Boring Location Diagram, and additional borings are recommended to determine final geotechnical design recommendations for this phase of the project once the remaining shopping mall buildings are demolished.
- We recommend that ECS be provided the opportunity to review the foundation plans and earthwork specifications to verify that our recommendations have been properly interpreted and implemented. ECS should also be retained to perform the construction material testing and observations required for this project, to verify that our recommendations have been satisfied.

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## 1.0 INTRODUCTION

The purpose of this study was to provide geotechnical information for the design of foundations, pavements, and stormwater management facilities for Titusville Resort and Destination, Phase 1 and 2. The project will include design and construction of one 4-story assisted living building and one 6-story multifamily residential building with an observation deck, along with a leasing/club house building and swimming pool, a 5-story hotel building with attached 1-story restaurant building and multiple 1-story commercial buildings with associated paved parking, drive areas and stormwater areas, rain garden and bioswales.

Our services were provided in general accordance with our Proposal No. 56-0964, dated February 28, 2024, and as authorized by you on March 12, 2024, which includes our Terms and Conditions of Service.

This report contains the procedures and results of our subsurface exploration and laboratory testing programs, review of existing site conditions, engineering analyses, and recommendations for the design and construction of the project.

The report includes the following items:

- A brief review and description of our field and laboratory test procedures and the results of testing conducted.
- A review of surface topographical features and site conditions.
- A review of area and site geologic conditions.
- A review of subsurface soil stratigraphy with pertinent available physical properties.
- Final copies of our soil boring logs for pre- and post-demolition phases.
- Recommendations for foundation design parameters, including our estimate of the performance of the foundation system. Updated recommendations include the results of pressuremeter testing for Buildings F, G and H.
- Swimming pool recommendations
- General recommendations for pavement design.
- Stormwater pond considerations and the results of permeability testing.
- Recommendations for site preparation and construction of compacted fills, including an evaluation of on-site soils for use as compacted fills.

## 2.0 PROJECT INFORMATION

### 2.1 PROJECT LOCATION/CURRENT SITE USE

The project site is located at 3550 South Washington Avenue, Titusville, Florida. The site was bordered to the north and south by residential properties, to the east by South Washington Avenue (US Highway 1) and to the west by South Hopkins Avenue. The general site location is shown below; the aerial photograph is showing site conditions as they existed pre-demolition.



Site Location

At the time of our exploration, the site was developed with the western portion of the previously existing 286,348 SF single story shopping mall building; the eastern half of the mall building in the area of proposed Buildings F, G and H (Phases 1 and 2) had been demolished. Asphalt paved parking and drive areas still existing around the existing/former building locations. Based on available site survey information provided to ECS, the site elevation in the area of the current borings was approximately El. 11, and remaining site areas ranged from approximately El. 8 to 11.

### 2.2 PAST SITE HISTORY/USES

ECS has reviewed aerial photographs of the subject site on Google Earth. The aerial photographs reviewed were dated 1984, 1994, 1999, 2002, 2003, 2004, 2005, 2006, 2007, 2009, 2010, 2012, 2013, 2014, 2016, 2017 and 2020. The 1984 aerial photograph shows the site developed with the current mall structures. The 1999 through 2020 aerial photographs showed no major changes in the site features.

### 2.3 SOIL SURVEY MAPPING

Based on the Web Soil Survey for Brevard County, Florida, as prepared by the U.S. Department of Agriculture Natural Resource Conservation Service, the predominant soil types existing within the site area are described in the following table. The site area is illustrated superimposed on the USDA-NRCS Soil Survey Map included as the following figure:

**Web Soil Survey Data**

Soil Type	Constituents	Drainage Class	Water Table
50 - Pomello-Urban Land Complex	Sand	Moderately Well drained	About 24 to 42 inches
69 - Urban Land, 0 to 2 percent slopes	Sand	Well Drained	-

**Urban Land:**

Urban land (Ur) consists of areas that are 60 to more than 75 percent covered with streets, buildings, large parking lots, shopping centers, industrial parks, airports, and related facilities. Unoccupied areas, mostly lawns, parks, vacant lots, and playgrounds, are Astatula, Paola, Myakka, St. Lucie, Immokalee, Pomello, Cocoa, and Ca-naveral soils in tracts too small to be mapped separately. Not assigned to a capability unit, range site, or woodland group.

Soil mapping of the site vicinity included soil types and numbers are presented in figure below, obtained from the USDA Web Soil site.



**Site Soil Survey**

**2.4 PROPOSED CONSTRUCTION**

We understand the proposed construction includes one 4-story assisted living building and one 6-story multifamily residential building along with a leasing/club house building and swimming pool, a 5-story hotel building with attached 1-story restaurant building and multiple 1-story commercial buildings with associated paved parking, drive areas and stormwater areas, rain garden and bioswales. We were provided by CES Design Group, Inc. estimated structural loading for the assisted living/multifamily residential buildings (Buildings F and G), of 40 kips per linear foot (klf) maximum wall and 300-kip maximum column loads. For the proposed hotel building (Building F), we have presumed maximum wall, column, and floor loads of 30 klf, 500 kips, and 250 pounds per square foot (psf), respectively. We also expect that less than 2 feet of fill (and only nominal cuts) will be required to achieve final grades in structural areas.

The following information explains our understanding of the planned development including proposed buildings and related infrastructure.

**Design Values for Residential Apartment Buildings G and H**

SUBJECT	DESIGN INFORMATION / EXPECTATIONS
# of Buildings	2
# of Stories	6-Story Maximum
Usage	Assisted Living/Multifamily Residential
Framing	Reinforced concrete with some steel framing and concrete slab on grade (provided)
Column Loads	300 kips (Full Dead and Factored Live) (provided)
Wall Loads	40 kips per linear foot (klf) maximum (provided)
Floor Loads	250 pounds per square foot (psf) maximum (assumed)

**Design Values for Restaurant and Commercial Buildings – Phase 1 and 3**

SUBJECT	DESIGN INFORMATION / EXPECTATIONS
# of Buildings	3
# of Stories	1- to 2-Story Maximum
Usage	Commercial
Framing	Masonry and/or wood-frame with concrete slab-on-grade (assumed)
Column Loads	Estimated 50 kips (Full Dead and Factored Live) (assumed)
Wall Loads	Estimated 3 kips per linear foot (klf) maximum (assumed)
Floor Loads	150 pounds per square foot (psf) maximum (assumed)

**Design Values for Hotel Building F**

SUBJECT	DESIGN INFORMATION / EXPECTATIONS
# of Stories	5-Story Maximum
Usage	Hotel
Framing	Reinforced concrete with some steel framing and concrete slab on grade (provided)
Column Loads	Estimated 500 kips (Full Dead and Factored Live) (assumed)
Wall Loads	Estimated 30 kips per linear foot (klf) maximum (assumed)
Floor Loads	250 pounds per square foot (psf) maximum (assumed)

\*If the provided and assumed structural loads differ from final design loads, this report needs to be revised to update and/or modify our foundation recommendations, bearing capacity, and settlement calculations.

### 3.0 FIELD EXPLORATION AND LABORATORY TESTING

Our exploration procedures are explained in greater detail in Appendix B including the insert titled Subsurface Exploration Procedures. Our scope of exploration work included drilling the following:

**Pre-demolition scope -**

- Standard Penetration Test (SPT) Borings B-01 to B-09, P-01 and PB-01 to PB-06, and Auger Borings R-01 to R-07. Borings PB-03 to PB-05 were performed in the Phase 3 area of the proposed development.

**Post-demolition scope -**

- SPT Borings BF-01 to BF-07 along with performing pressuremeter testing at three locations (PM-01 to PM-03) on the site (see Section 3.2, Pressuremeter Testing).

Our borings were located with a handheld GPS unit and their approximate locations are shown on the Boring Location Diagram (Figure 2) in Appendix A.

#### 3.1 SUBSURFACE CHARACTERIZATION FROM BORINGS

The subsurface conditions encountered were generally consistent with published geological mapping. The following sections provide generalized characterizations of the soil strata. Please refer to the boring logs in Appendix B.

#### Subsurface Stratigraphy of SPT Borings

Approximate Depth Range (ft)	Stratum	Description	Ranges of SPT <sup>(1)</sup> N-values (bpf)
0 – 0.4 to 0.7	N/A	Topsoil <sup>(2)</sup>	---
0.4 to 0.7 – 35 to 50	I	Very Loose to Very Dense Fine Sand (SP), Fine Sand with Claye (SP-SC) and Fine Sand with Silt (SP-SM), often contains significant shell fragments	4 to 53
35 to 50 – 65 to 75	II	Medium Dense to Dense Fine Sand with Clay (SP-SC) and Clayey Fine Sand (SC), often contains significant shell fragments	7 to 37
65 to 70 – 75	III	Soft to Hard, Limestone <sup>(2)</sup>	22 to 54

Notes: (1) Standard Penetration Test.

(2) Topsoil or limestone were not encountered in the post-demolition Borings BF-01 to BF-07.

**Subsurface Stratigraphy of Pavement (Auger) Borings**

Approximate Depth Range (ft)	Stratum	Description
0 – 0.4 to 0.7	N/A	Topsoil
0.4 to 0.7 – 6	I	Fine Sand (SP)

**3.2 PRESSUREMETER TESTING**

To optimize the net allowable bearing pressures for foundation design at the site, ECS has performed pressuremeter testing. In the pressuremeter test, a radially expanding cylindrical probe is directly pushed into the soil at the desired test depth. After insertion, the probe is expanded incrementally against the side of the surrounding soil with pressurized liquid. Each pressure increment is maintained until the readings stabilize. The pressure increments are continued until failure of the soil is reached. The change in diameter of each hole under each pressure increment is measured by the volume change in the center portion of the probe.

By plotting the probe volume versus pressure, a stress-volumetric strain curve is obtained. From this curve, the pressuremeter modulus is determined, which is derived from the slope of the stress-volumetric strain curve in the elastic zone. The pressuremeter modulus is used to estimate the soil elastic modulus, which is used to estimate foundation (and other loaded area) settlements. The Pressuremeter Testing was performed at the locations PM-01 to PM-03 (see Figure 2, Appendix A). ECS notes that the test results from location PM-02 were not considered reliable; therefore, only the results from PM-01 and PM-03 were used to determine net allowable bearing capacity for design recommendations. The results of the pressuremeter testing are presented in Appendix D.

**3.3 GROUNDWATER OBSERVATIONS**

Groundwater levels were measured during our field exploration and are presented in our boring logs in Appendix B. Groundwater depths measured at the time of drilling ranged from 3.5 to 6 feet below the ground surface. Variations in the long-term water table may occur as a result of changes in precipitation, evaporation, surface water runoff, construction activities, and other factors.

**Estimated Seasonal High Groundwater**

The normal seasonal high groundwater level is affected by a number of factors. The drainage characteristics of the soils, land surface elevation, relief points such as drainage ditches, lakes, rivers, swamp areas, etc., and distance to relief points are some of the more important factors influencing the seasonal high groundwater level.

Based on our interpretation of the site conditions, including the boring logs and Web Soil Survey, we estimate the normal seasonal high groundwater level at the boring locations to be up to 1.5 feet higher than the depths encountered in our borings, as shown on the Boring Logs. It is possible that groundwater levels may exceed the estimated normal seasonal high groundwater level as a result of significant or prolonged rains.

### **3.4 LABORATORY TESTING**

Each sample was visually classified on the basis of texture and plasticity in accordance with ASTM D2488 Standard Practice for Description and Identification of Soils (Visual-Manual Procedures) and including USCS classification symbols, and ASTM D2487 Standard Practice for Classification for Engineering Purposes (Unified Soil Classification System (USCS)). After classification, the samples were grouped in the major zones noted on the boring logs in Appendix B. The group symbols for each soil type are indicated in parentheses along with the soil descriptions. The stratification lines between strata on the logs are approximate; in situ, the transitions may be gradual.

The laboratory testing consisted of selected tests performed on samples obtained during our field exploration operations. Classification and index property tests were performed on representative soil samples and included percent fines tests (ASTM D1140), moisture content tests (ASTM D2216), Atterberg Limits (ASTM D4318) and falling head permeability tests (ASTM D5084-16a).

## 4.0 DESIGN RECOMMENDATIONS

### 4.1 FOUNDATION AREA PREPARATION

Very loose to loose soils sands were encountered in the upper 2 to 10 feet below the existing ground surface at some of the boring locations. As outlined in Section 5.1.4, a heavy vibratory roller should be used to compact the surface soils below the proposed footings. To further compact the soil below the proposed hotel footprint, we recommend over-excavating the upper 3 feet of soil within foundation areas before compaction of the subgrade with the heavy vibratory roller. After subgrade compaction, the over-excavated sandy soils can be reused as the compacted structural backfill. Dynamic cone penetrometer (DCP) soundings, performed by hand, should also be performed subsequent to the surface soil heavy compaction operations to confirm densification of the sands within the upper 4 feet of the footing bearing elevations. This recommendation is particularly important due to the higher allowable bearing pressure provided herein as a result of the pressuremeter testing performed by ECS.

### 4.2 FOUNDATION DESIGN

Provided subgrades and structural fills are prepared as recommended in this report, including necessary over-excavation at the hotel location, proof-rolling, and compaction at existing subgrade or footing bottom elevation (hotel area) with a heavy vibratory drum roller – followed by verification (Quality Control) testing, the proposed structures can be supported by shallow column and continuous wall footings using the following parameters:

#### Apartment Buildings G and H Foundation Parameters – Phase 1

Design Parameter	Column Footing	Wall Footing
Minimum Width	24 inches	24 inches
Minimum Footing Embedment Depth (below slab or finished grade)	24 inches	18 inches
Estimated Maximum Total Settlement <sup>1</sup>	1 inch	1 inch
Estimated Maximum Differential Settlement <sup>2</sup>	Less than ½ inches between columns	Less than ½ inches over 50 feet
Net Allowable Bearing Pressure <sup>3</sup>	<b>3,000 psf at 18-inch embedment depth (walls) 5,000 psf at 24-inch embedment (columns and walls)</b>	
Acceptable Bearing Soil Material	Medium Dense Fine Sand (SP) – Stratum I or Compacted Fill	

### Hotel Building F Foundation Parameters – Phase 2

Design Parameter	Column Footing	Wall Footing
Minimum Width	24 inches	24 inches
Minimum Footing Embedment Depth (below slab or finished grade)	24 inches	18 inches
Estimated Maximum Total Settlement <sup>1</sup>	1 inch	1 inch
Estimated Maximum Differential Settlement <sup>2</sup>	Less than ½ inches between columns	Less than ½ inches over 50 feet
Net Allowable Bearing Pressure <sup>3</sup>	<b>3,000 psf at 18-inch embedment depth (walls) 5,000 psf at 24-inch embedment (columns and walls)</b>	
Acceptable Bearing Soil Material	Medium Dense Fine Sand (SP) – Stratum I or Compacted Fill	

### Commercial Buildings Foundation Parameters – Phase 1

Design Parameter	Column Footing	Wall Footing
Minimum Width	24 inches	18 inches
Minimum Footing Embedment Depth (below slab or finished grade)	18 inches	18 inches
Estimated Maximum Total Settlement <sup>1</sup>	1 inch	1 inch
Estimated Maximum Differential Settlement <sup>2</sup>	Less than ½ inches between columns	Less than ½ inches over 50 feet
Net Allowable Bearing Pressure <sup>3</sup>	2,500 psf	
Acceptable Bearing Soil Material	Medium Dense Fine Sand (SP) – Stratum I or Compacted Fill	

1. Based on estimated structural loads. If final loads are different, ECS must be contacted to update foundation recommendations and settlement calculations.
2. Based on maximum column/wall loads and variability in borings. Differential settlement can be re-evaluated once the foundation plans are more complete.
3. Net allowable bearing pressure is the applied pressure in excess of the surrounding overburden soils above the base of the foundation.

Depending on the final floor elevations of the buildings, we anticipate that most of the soils at the foundation bearing elevation are anticipated to be suitable for support of the proposed structures, after preparation in accordance with Section 5.0 of this report. The bearing level soils, after compaction, should exhibit densities equivalent to 95 percent of the modified Proctor maximum dry density (ASTM D 1557) to a depth of at least one foot below foundation bearing levels.

For turn down slabs and interior wall footings the minimum width should also be 18 inches, however the sloped transition portion of the turn-down may be included when determining the footing width. Even though the maximum allowable soil bearing pressure may not be achieved, these width recommendations should control the size of the foundations.

#### 4.3 SLABS ON GRADE

The floor slabs can be constructed as a slab-on-ground, provided the site is prepared as outlined in Section 5.0. A minimum clearance of 2 feet is recommended between the estimated seasonal high groundwater table and the bottom of the floor slab. It is recommended the floor slab bearing soils be covered with an impervious membrane to reduce moisture entry and floor dampness. A 6-mil thick plastic membrane is commonly used for this purpose. Care should be exercised not to tear

large sections of the membrane during placement of reinforcing steel and concrete. In addition, we recommend that a minimum separation of two feet be maintained between the finished floor levels and the estimated normal seasonal high groundwater level.

**Subgrade Modulus:** Provided the placement of structural fill per the recommendations discussed herein, the slab may be designed assuming a modulus of subgrade reaction,  $k_1$  of 150 pci (lbs/cu. inch). The modulus of subgrade reaction value is based on a 1 ft by 1 ft plate load test basis.

#### 4.4 PAVEMENTS

Based on the results of our exploration, we consider the subsurface conditions at the site favorable for support of a flexible or rigid pavement section when constructed on properly prepared subgrade soils as outlined in Section 5.0 of this report. Typical pavement sections used in northeast Florida are presented in the following sections. If requested, we can prepare a project-specific pavement design if specific traffic data is provided.

In general, heavy duty sections are areas that will be subjected to trucks, buses, or other similar vehicles including main drive lanes of the development. Light duty sections are appropriate for vehicular traffic and parking areas.

##### 4.4.1 Flexible Pavement Recommendations

TYPICAL FLEXIBLE PAVEMENT SECTIONS		
MATERIAL	LIGHT DUTY	HEAVY DUTY
Asphaltic Concrete Surface Course (SP-9.5 or Type S)	1.5 inches	2 inches
Limerock Base	6 inches	8 inches
Stabilized Subgrade	12 inches	12 inches

**Base and Subgrade:** The limerock base course should have a minimum Limerock Bearing Ratio (LBR) of 100 and should be compacted to 98 percent of the modified Proctor maximum dry density (ASTM D 1557) value.

The subgrade material should have a minimum LBR of 40 and be compacted to 98 percent of the modified Proctor maximum dry density (ASTM D1557) value.

**Underdrains:** Satisfactory pavement life is dependent on dry/strong pavement support provided by the base and subgrade courses. Accordingly, a minimum clearance of 2 feet must be maintained between the normal seasonal high groundwater table and the bottom of the limerock base layer. Depending on final pavement grades, FDOT Type I or II underdrains may be required to maintain dry base and subgrade materials.

##### 4.4.2 Rigid Pavement Recommendations

Our recommendations for slab thickness for standard duty and heavy duty concrete pavements are based on a) subgrade soils densified to 98 percent of the modified Proctor maximum dry density (ASTM D1557) b) modulus of subgrade reaction ( $k$ ) equal to 200 pounds per cubic inch, c) a 20 year design life.

TYPICAL RIGID PAVEMENT SECTIONS		
	LIGHT DUTY	HEAVY DUTY
Minimum Concrete Thickness	5 inches	6 inches
Maximum Control Joint Spacing	10 feet x 10 feet	12 feet x 12 feet
Recommended Sawcut Depth	1 ¼ inches	1 ½ inches

We recommend using concrete with a minimum 28-day compressive strength of 4,000 psi and a minimum 28-day flexural strength (modulus of rupture) of at least 600 pounds per square inch, based on 3rd point loading of concrete beam test samples. Layout of the sawcut control joints should form square panels. The joints should be sawed within six hours of concrete placement or as soon as the concrete has developed sufficient strength to support workers and equipment. We recommend allowing ECS to review and comment on the final concrete pavement design, including section and joint details (type of joints, joint spacing, etc.), prior to the start of construction.

For further details on concrete pavement construction, please reference the “Guide to Jointing on Non-Reinforced Concrete Pavements” published by the Florida Concrete and Products Associates, Inc., and “Building Quality Concrete Parking Areas”, published by the Portland Cement Association.

#### 4.5 STORMWATER MANAGEMENT FACILITIES

##### 4.5.1 Soil Permeability Rate

The results of the permeability tests indicated the following vertical/horizontal permeabilities:

##### Laboratory Permeability Results

Test Location	Soil Type	Test Depth (feet)	Measured Mean Permeability (ft/day) $K_m$	Estimated Horizontal Permeability (ft/day) $K_h$	Estimated Vertical Permeability (ft/day) $K_v$
R-2	SP	4 to 6	19.2	19.2	19.2
R-3	SP	4 to 6	16.0	16.0	16.0
P-1	SP-SM	4 to 6	2.2	3.3	2.2
BF-05	SP	4 to 6	12.3	12.3	12.3
BF-06	SP-SM	4 to 6	10.8	13.2	8.8
BF-07	SP-SM	4 to 6	3.8	4.7	3.1

Note the laboratory permeability tests performed are remolded samples from our soil boring samples. For pond design calculations, we recommend an appropriate factor of safety be applied to the above permeability values.

##### 4.5.2 Borrow Suitability

Based on the boring results and classification of the soil samples, the predominant fine sand, fine sand with silt and fine sand with clay (SP, SP-SM, SP-SC), as encountered in the borings, are able to

be used as structural fill soil. Clayey sand (SC) soils may be encountered in the near surface materials at the site and are not recommended for use as structural fill without the approval of the geotechnical engineer.

It should be anticipated that the soils in the proposed pond areas below the groundwater level will have moisture contents in excess of the Modified Proctor optimum moisture content. This will require stockpiling or spreading to drain the excess moisture. Generally, the wet soils should be dried to bring the soil moisture content within  $\pm 2$  percent of the soil's optimum moisture content to facilitate placement and compaction.

#### **4.6 BELOW GRADE POOL DESIGN RECOMMENDATIONS**

##### **4.6.1 General**

Based on the results of the boring performed within the proposed swimming pool structure area, it is our opinion that the soils encountered at the boring locations are adaptable for support of the proposed pool construction. We anticipate that the pool structures will exert little or no net downward pressure on the soils; rather, the structure may be subject to hydrostatic uplift pressure when the pool is empty. Below-grade structures should be designed to resist lateral earth pressures and hydrostatic uplift pressures appropriate for their depth below existing grade and wet season groundwater table.

The walls of the structure should be designed to resist at-rest lateral earth pressures, with equivalent fluid densities above and below the water table being as follows:

- Above Water Table - Equivalent Fluid Density 60 pcf
- Below Water Table - Equivalent Fluid Density 90 pcf

For wall design purposes, the groundwater level should be assumed to be at prevailing grade.

##### **4.6.2 Uplift Protection**

When the water level within below-grade pool structures is maintained at or above the surrounding groundwater level, no net buoyancy will occur to the structure. However, a positive means of uplift protection will be necessary when the pool structure is drained for maintenance or as water levels fluctuate within the pool. Hydrostatic uplift forces can be resisted in several ways including:

1. Addition of dead weight to the structure.
2. Mobilizing the dead weight of the soil surrounding the structure through extension of footings outside the perimeter of the structure.
3. Use of a permanent gravity or mechanical dewatering system that is operated only when the structure is to be drained.
4. Use of pressure relief valves in the bottom of the pool in combination with one or more of the above methods.

We anticipate that options one or two may be needed for this construction depending on the depth of the pools. At your request, we would be pleased to assist you in evaluating uplift protection requirements.

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## 5.0 SITE CONSTRUCTION RECOMMENDATIONS

### 5.1 SUBGRADE PREPARATION

#### 5.1.1 Stripping and Grubbing

Prior to construction, the location of existing underground utilities within the construction area should be established. Provisions should then be made to relocate interfering utilities to appropriate locations. Underground pipes that are not properly removed or plugged may serve as conduits for subsurface erosion, which may subsequently lead to excessive settlement of overlying structures.

The "footprint" of the proposed buildings plus a minimum additional margin of 5 feet, and of the hardscape areas (parking/driveway) plus a minimum additional margin of 3 feet, should be stripped of all surface vegetation, stumps, demolition debris, organic topsoil, concrete, asphalt or other deleterious materials. During grubbing operations, roots with a diameter greater than 0.5-inch, stumps, or small roots in a concentrated state, should be grubbed and completely removed.

Based on the results of our field exploration, it should be anticipated that 1 inch to 1.5 inches of asphalt and 3 to 6 inches of limerock may be encountered across the site. The actual depths of unsuitable soils and materials should be determined by ECS using visual observation and judgment during earthwork operations. Any topsoil removed from the building and parking/drive areas can be stockpiled and used subsequently in non-structural areas.

#### 5.1.2 Proofrolling

After removing all unsuitable surface materials, cutting to the proposed grade, and prior to the placement of any structural fill or other construction materials, the exposed subgrade should be evaluated by the Geotechnical Engineer or authorized representative. The exposed subgrade should be thoroughly proofrolled with previously approved construction equipment having a minimum axle load of 20 tons (e.g. fully loaded tandem-axle dump truck). The areas subject to proofrolling should be traversed by the equipment in two perpendicular (orthogonal) directions with overlapping passes of the vehicle under the observation of the Geotechnical Engineer or authorized representative. This procedure is intended to assist in identifying any localized yielding materials. In the event that unstable or "pumping" subgrade is identified by the proofrolling, those areas should be marked for repair prior to the placement of any subsequent structural fill or other construction materials. Methods of repair of unstable subgrade, such as undercutting or moisture conditioning, should be discussed with the Geotechnical Engineer to determine the appropriate procedure with regard to the existing conditions causing the instability. A test pit(s) may be excavated to explore the shallow subsurface materials in the area of the instability to help in determining the cause of the observed unstable materials and to assist in the evaluation of the appropriate remedial action to stabilize the subgrade.

#### 5.1.3 Temporary Groundwater Control

Because of the need for densification of the soils within the upper 2 feet below the stripped surface, temporary groundwater control measures may be required if the groundwater level is within 2 feet below the stripped and grubbed surface at the time of construction. Should groundwater control measures become necessary, dewatering methods should be determined by the contractor. We recommend the groundwater control measures, if necessary; remain in place until compaction of the existing soils is completed. The dewatering method should be maintained until backfilling has reached a height of 2 feet above the groundwater level at the time of construction. The site should be graded to direct surface water runoff from the construction area.

Note that discharge of produced groundwater to surface waters of the state from dewatering operations or other site activities is regulated and requires a permit from the State of Florida Department of Environmental Protection (FDEP). This permit is termed a Generic Permit for the Discharge of Produced Groundwater From Any Non-Contaminated Site Activity. If discharge of produced groundwater is anticipated, we recommend sampling and testing of the groundwater early in the site design phase to prevent project delays during construction. ECS can provide the sampling, testing, and professional consulting required to evaluate compliance with the regulations.

#### 5.1.4 Subgrade Compaction

After completing the clearing and stripping operations and installing the temporary groundwater control measures (if required), the exposed surface in building and pavement areas should be compacted with a heavy vibratory roller having a minimum static, at-drum weight on the order of 15 to 20 tons. An approved heavy vibratory roller should be used to compact the surface soils and enable densification of near-surface very loose to loose soils. Because of the relatively dry condition of the surficial fine sands, these soils will likely need to be watered down to increase their moisture content to near their optimum value that will best facilitate compaction. With the soils properly moisture conditioned, our experience indicates that at least eight overlapping passes in each direction of the vibratory roller should achieve the desired densification of the surficial loose fine sands to depths of 2 to 10 feet. Typically, the material should exhibit moisture contents within  $\pm 2$  percentage points of the modified Proctor optimum moisture content (ASTM D1557) during the compaction operations. Compaction should continue until densities of at least 95 percent of the modified Proctor maximum dry density (ASTM D1557) have been achieved within the upper 2 feet of the compacted natural soils at the site.

**To further compact the soil below the proposed hotel footprint, we recommend over-excavating the upper 3 feet of soil before compaction of the subgrade. The heavy vibratory roller and methodology for subgrade compaction following over-excavation should be as previously discussed herein.** We recommend that temporary groundwater control measures within this area be implemented so that the groundwater table is maintained a depth of 4 feet below the excavated subgrade bottom at the time of compaction operations. After subgrade compaction, the over-excavated sandy soils can be reused as the compacted structural backfill.

Should the bearing level soils experience pumping and soil strength loss during the compaction operations, compaction work should be immediately terminated, and (1) the disturbed soils should be removed and backfilled with compacted structural fill, or (2) the excess moisture content within the disturbed soils should be allowed to dissipate before recompacting.

Care should be exercised to avoid damaging any nearby structures while the compaction operation is underway. Prior to commencing compaction, occupants of adjacent structures should be notified, and the existing conditions of the structures should be documented with photographs and survey (if deemed necessary). Compaction should cease if deemed detrimental to adjacent structures, and ECS should be contacted immediately. We recommend the vibratory roller remain a minimum of 50 feet from existing structures. Within this zone, use of a track-mounted bulldozer, or a vibratory roller operating in the static mode, is recommended.

## 5.2 EARTHWORK OPERATIONS

### 5.2.1 Structural Backfill and Fill Soils

Structural fill is defined as a non-plastic, inorganic, granular soil having less than 10 percent material passing the No. 200 mesh sieve and containing less than 4 percent organic material. The fine sand

and fine sand with silt or fine sand with clay, without roots, as encountered in the borings, are suitable as fill materials and, with proper moisture control, should densify using conventional compaction methods. Soils with more than 10 to 12 percent passing the No. 200 sieve will be more difficult to compact, due to their nature to retain soil moisture, and may require drying. Clayey sand (SC) soils may be encountered in the near surface materials at the site and are not recommended for use as structural fill without the approval of the geotechnical engineer.

**Structural Fill Compaction Requirements:** Materials satisfactory for use as structural fill should consist of soils with the following compaction requirements.

<b>STRUCTURAL FILL COMPACTION REQUIREMENTS</b>	
<b>Subject</b>	<b>Requirement</b>
Compaction Standard	Modified Proctor, ASTM D1557
Required Compaction	95% of Max. Dry Density (general structural fill) 98% of Max. Dry Density (upper one foot below the proposed pavement base course)
Loose Thickness prior to compaction	12 inches if vibratory drum roller compaction equipment is used 8 inches if vibratory drum roller is used in static mode 8 inches if track-mounted compaction equipment is used 6 inches if hand-held compaction equipment is used

Fill materials should not be placed on excessively wet soils. Excessively wet soils should be scarified, aerated, and moisture conditioned. Proper drainage should be maintained during the earthwork phases of construction to prevent ponding of water which has a tendency to degrade subgrade soils. The contractor should minimize dusting or implement dust control measures, as required.

We recommend that the grading contractor have equipment on site during earthwork for both drying and wetting fill soils. Moisture control may be difficult during extended periods of rain. The control of moisture content of soils containing more than 10% fines may be difficult when these soils become wet. Further, such soils are easily degraded by construction traffic when the moisture content is elevated.

**5.2.2 Foundation Areas**

After satisfactory placement and compaction of the required structural fill, the foundation areas may be excavated to the planned bearing levels. The foundation bearing level soils, after compaction, should exhibit densities equivalent to 95 percent of the modified Proctor maximum dry density (ASTM D1557) to a depth of one foot below the bearing level. For confined areas, such as the footing excavations, any compactive effort should be provided by a lightweight vibratory sled or roller having a total weight on the order of 500 to 2,000 pounds. Within the hotel and apartment building areas, Dynamic Cone Penetrometer (DCP) soundings, performed by hand, should also be performed subsequent to the surface soil heavy compaction operations to confirm densification of the sands within the upper 4 feet of the footing bearing elevations.

**5.2.3 Flexible Pavement Areas**

After completing the clearing/stripping operations in the pavement areas, any underlying clayey sands (and sandy clays) that are within 2 feet of the bottom of the pavement base should be over-excavated from within the pavement areas. Structural backfill and fill required to achieve the finish pavement grades then can be placed and compacted as described in Sections 5.2.1.

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#### 5.2.4 Rigid Pavement Areas

For a concrete pavement subgrade, we recommend using clean fine sand (SP), compacted to at least 98 percent of modified Proctor test maximum dry density (ASTM D1557) without additional stabilization.

#### 5.3 UTILITY INSTALLATIONS

**Utility Subgrades:** The soil borings within proposed pavement areas predominantly encountered fine sands, fine sands with clay (SP-SC) and fine sands with silt (SP, SP-SM). It is our opinion that these soils are suitable bedding soils for pipelines and utility structures and replaced with compacted structural fill as described in Section 5.2.1 above. Where clayey sand (SC) or silty sand (SM) soils are encountered and it is determined that they contain more than 20 percent fines, these soils should be over-excavated to a depth of 12 inches below pipe invert or 24 inches below manhole structure base, and should be replaced with an approved structural fill.

Alternatively, a medium-duty woven geotextile, such as Mirafi 600X or equivalent, may be used as a separation barrier between the compacted backfill and the clayey/silty soils. If a woven geotextile is used, then no overexcavation is necessary for the pipeline, and the depth of overexcavation for the utility manholes may be reduced to 12 inches. The geotextile should be placed in the excavation bottom and along the sides above the silty/clayey soils creating a barrier between these soils and the sand backfill to preclude contamination of the backfill.

**Utility Backfilling:** Backfill placed around the pipe, and to a height of 2 feet above the top of pipe, should be placed in 6-inch lifts. Each lift should be compacted with hand-held equipment to 98 percent of the soil's Modified Proctor (ASTM D1557) maximum dry density. Backfill placed above the 2-foot zone above the top of pipe elevation may be placed in 12-inch lifts and compacted with heavier equipment. Typically, the backfill soil should exhibit moisture contents within  $\pm 2$  percent of the soil's optimum moisture content as determined from the Proctor test. Care should be taken to avoid damaging the pipe during compaction operations.

Backfill placed around utility structures should be placed in 6-inch thick lifts, and compacted with hand-held equipment to the same in-place soil density stated above. Heavy equipment should not be used within 5 feet of the structures to prevent overstressing of the structure walls.

**Utility Excavation Dewatering:** Based on the groundwater depths encountered in our borings, groundwater will likely be encountered by utility excavations which extend below existing grades. It is expected that removal of groundwater will be required, especially for deeper utility excavations. The contractor should submit a dewatering plan prior to installing the site utilities.

**Excavation Safety:** All excavations and slopes should be made and maintained in accordance with OSHA excavation safety standards. The contractor is solely responsible for designing and constructing stable, temporary excavations and slopes and should shore, slope, or bench the sides of the excavations and slopes as required to maintain stability of both the excavation sides and bottom. The contractor's responsible person, as defined in 29 CFR Part 1926, should evaluate the soil exposed in the excavations as part of the contractor's safety procedures. In no case should slope height, slope inclination, or excavation depth, including utility trench excavation depth, exceed those specified in local, state, and federal safety regulations. ECS is providing this information solely as a service to our client. ECS is not assuming responsibility for construction site safety or the contractor's activities; such responsibility is not being implied and should not be inferred.

**Erosion Control:** The surface soils may be erodible. Therefore, the Contractor should provide and maintain good site drainage during earthwork operations to maintain the integrity of the surface soils. All erosion and sedimentation controls should be in accordance with sound engineering practices and local requirements.

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## 6.0 CLOSING

Our geotechnical exploration has been performed, our findings obtained, and our recommendations prepared, in accordance with generally accepted geotechnical engineering principles and practices. ECS is not responsible for any independent conclusions, interpretation, opinions, or recommendations made by others based on the data contained in this report.

Our scope of services was intended to evaluate the soil conditions within the zone of soil influenced by the foundation system. Our scope of services does not address geologic conditions, such as sinkholes or soil conditions existing below the depth of the soil borings.

ECS is currently performing environmental consulting service for the project. The environmental findings will be issued in a separate report.

If any of the project description information discussed in this report is inaccurate, either due to our interpretation of the documents provided or site or design changes that may occur later, ECS should be contacted immediately in order that we can review the report in light of the changes and provide additional or alternate recommendations as may be required to reflect the proposed construction.

We recommend that ECS be allowed to review the project's plans and specifications pertaining to our work so that we may ascertain consistency of those plans/specifications with the intent of the geotechnical report.

Field observations, monitoring, and quality assurance testing during earthwork and foundation installation are an extension of and integral to the geotechnical design recommendation. We recommend that the owner retain these quality assurance services and that ECS be allowed to continue our involvement throughout these critical phases of construction to provide general consultation as issues arise.

## **APPENDIX A – Diagrams & Reports**

Figure 1 - Site Location Diagram

Figure 2 – Boring Location Diagram

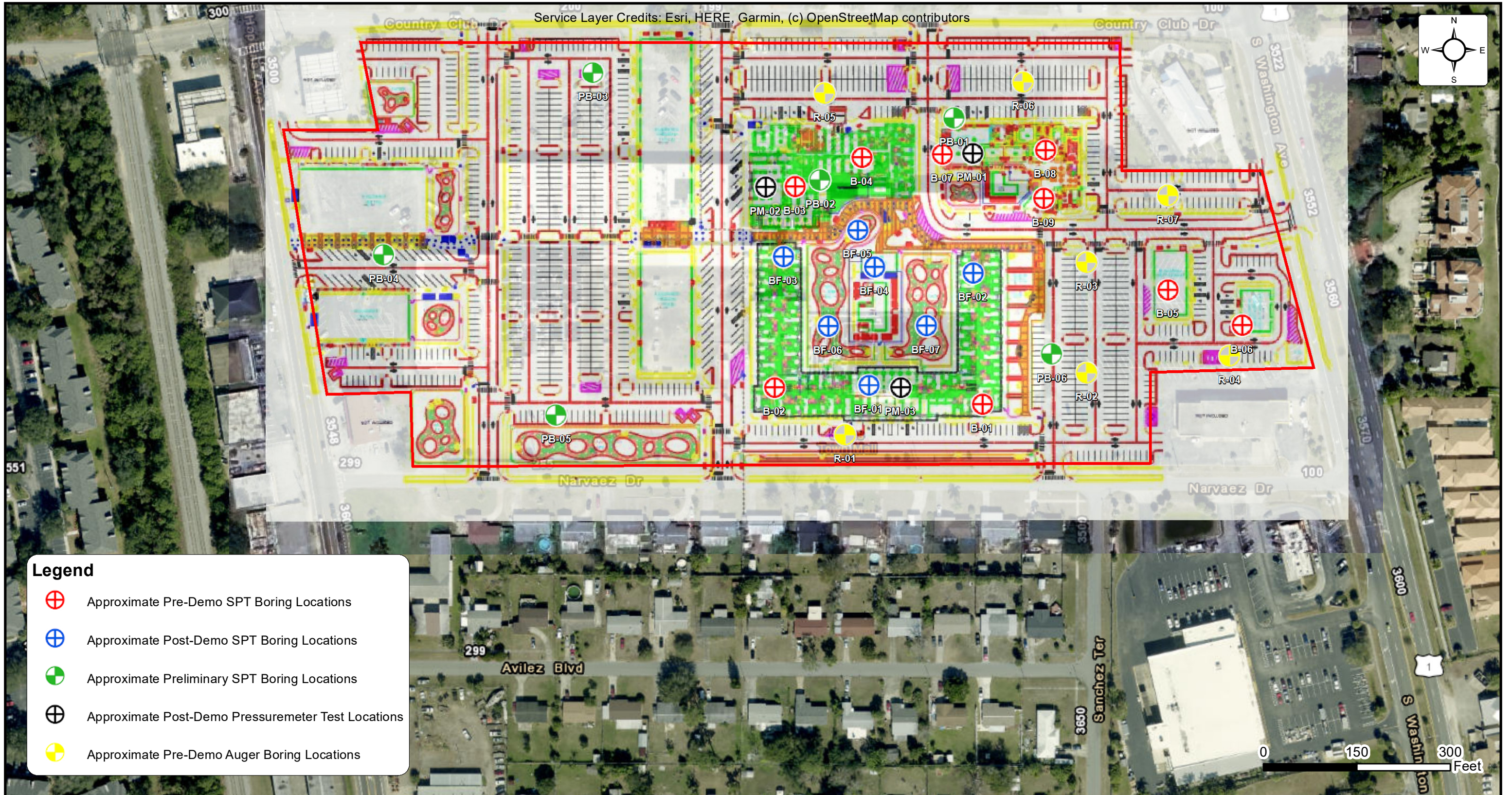


**SITE LOCATION DIAGRAM  
TITUSVILLE MALL REDEVELOPMENT**

**3550 S. WASHINGTON AVENUE, TITUSVILLE, FLORIDA**  
TITUSVILLE RESORT AND DESTINATION, LLC



ENGINEER	MK6
SCALE	AS NOTED
PROJECT NO.	56:1380-B
FIGURE	1 OF 2
DATE	4/26/2024



**Legend**

- Approximate Pre-Demo SPT Boring Locations
- Approximate Post-Demo SPT Boring Locations
- Approximate Preliminary SPT Boring Locations
- Approximate Post-Demo Pressuremeter Test Locations
- Approximate Pre-Demo Auger Boring Locations



# BORING LOCATION DIAGRAM TITUSVILLE MALL REDEVELOPMENT

**3550 S. WASHINGTON AVENUE, TITUSVILLE, FLORIDA**  
TITUSVILLE RESORT AND DESTINATION, LLC

ENGINEER	MK6
SCALE	AS NOTED
PROJECT NO.	56:1380-B
FIGURE	2 OF 2
DATE	5/14/2024

## **APPENDIX B – Field Operations**

Reference Notes for Boring Logs

Subsurface Exploration Procedure: Standard Penetration Testing (SPT)  
ASTM D1586

Subsurface Exploration Procedure: Hand Auger Borings ASTM D1452  
SPT Boring Logs  
Auger Boring Logs

# REFERENCE NOTES FOR BORING LOGS

MATERIAL <sup>1,2</sup>	
	<b>ASPHALT</b>
	<b>CONCRETE</b>
	<b>GRAVEL</b>
	<b>TOPSOIL</b>
	<b>VOID</b>
	<b>BRICK</b>
	<b>AGGREGATE BASE COURSE</b>
	<b>GW WELL-GRADED GRAVEL</b> gravel-sand mixtures, little or no fines
	<b>GP POORLY-GRADED GRAVEL</b> gravel-sand mixtures, little or no fines
	<b>GM SILTY GRAVEL</b> gravel-sand-silt mixtures
	<b>GC CLAYEY GRAVEL</b> gravel-sand-clay mixtures
	<b>SW WELL-GRADED SAND</b> gravelly sand, little or no fines
	<b>SP POORLY-GRADED SAND</b> gravelly sand, little or no fines
	<b>SM SILTY SAND</b> sand-silt mixtures
	<b>SC CLAYEY SAND</b> sand-clay mixtures
	<b>ML SILT</b> non-plastic to medium plasticity
	<b>MH ELASTIC SILT</b> high plasticity
	<b>CL LEAN CLAY</b> low to medium plasticity
	<b>CH FAT CLAY</b> high plasticity
	<b>OL ORGANIC SILT or CLAY</b> non-plastic to low plasticity
	<b>OH ORGANIC SILT or CLAY</b> high plasticity
	<b>PT PEAT</b> highly organic soils

DRILLING SAMPLING SYMBOLS & ABBREVIATIONS			
SS	Split Spoon Sampler	PM	Pressuremeter Test
ST	Shelby Tube Sampler	RD	Rock Bit Drilling
WS	Wash Sample	RC	Rock Core, NX, BX, AX
BS	Bulk Sample of Cuttings	REC	Rock Sample Recovery %
PA	Power Auger (no sample)	RQD	Rock Quality Designation %
HSA	Hollow Stem Auger		

PARTICLE SIZE IDENTIFICATION		
DESIGNATION	PARTICLE SIZES	
Boulders	12 inches (300 mm) or larger	
Cobbles	3 inches to 12 inches (75 mm to 300 mm)	
Gravel:	Coarse	¾ inch to 3 inches (19 mm to 75 mm)
	Fine	4.75 mm to 19 mm (No. 4 sieve to ¾ inch)
Sand:	Coarse	2.00 mm to 4.75 mm (No. 10 to No. 4 sieve)
	Medium	0.425 mm to 2.00 mm (No. 40 to No. 10 sieve)
	Fine	0.074 mm to 0.425 mm (No. 200 to No. 40 sieve)
Silt & Clay ("Fines")	<0.074 mm (smaller than a No. 200 sieve)	

COHESIVE SILTS & CLAYS		
UNCONFINED COMPRESSIVE STRENGTH, QP <sup>4</sup>	SPT <sup>5</sup> (BPF)	CONSISTENCY <sup>7</sup> (COHESIVE)
<0.25	<2	Very Soft
0.25 - <0.50	3 - 4	Soft
0.50 - <1.00	5 - 8	Firm
1.00 - <2.00	9 - 15	Stiff
2.00 - <4.00	16 - 30	Very Stiff
4.00 - 8.00	31 - 50	Hard
>8.00	>50	Very Hard

RELATIVE AMOUNT <sup>7</sup>	COARSE GRAINED (%) <sup>8</sup>	FINE GRAINED (%) <sup>8</sup>
Trace	≤5	≤5
With	10 - 20	10 - 25
Adjective (ex: "Silty")	25 - 45	30 - 45

GRAVELS, SANDS & NON-COHESIVE SILTS	
SPT <sup>5</sup>	DENSITY
<5	Very Loose
5 - 10	Loose
11 - 30	Medium Dense
31 - 50	Dense
>50	Very Dense

WATER LEVELS <sup>6</sup>	
	WL (First Encountered)
	WL (Completion)
	WL (Seasonal High Water)
	WL (Stabilized)

FILL AND ROCK			
FILL	POSSIBLE FILL	PROBABLE FILL	ROCK

<sup>1</sup>Classifications and symbols per ASTM D 2488-17 (Visual-Manual Procedure) unless noted otherwise.

<sup>2</sup>To be consistent with general practice, "POORLY GRADED" has been removed from GP, GP-GM, GP-GC, SP, SP-SM, SP-SC soil types on the boring logs.

<sup>3</sup>Non-ASTM designations are included in soil descriptions and symbols along with ASTM symbol [Ex: (SM-FILL)].

<sup>4</sup>Typically estimated via pocket penetrometer or Torvane shear test and expressed in tons per square foot (tsf).

<sup>5</sup>Standard Penetration Test (SPT) refers to the number of hammer blows (blow count) of a 140 lb. hammer falling 30 inches on a 2 inch OD split spoon sampler required to drive the sampler 12 inches (ASTM D 1586). "N-value" is another term for "blow count" and is expressed in blows per foot (bpf). SPT correlations per 7.4.2 Method B and need to be corrected if using an auto hammer.

<sup>6</sup>The water levels are those levels actually measured in the borehole at the times indicated by the symbol. The measurements are relatively reliable when augering, without adding fluids, in granular soils. In clay and cohesive silts, the determination of water levels may require several days for the water level to stabilize. In such cases, additional methods of measurement are generally employed.

<sup>7</sup>Minor deviation from ASTM D 2488-17 Note 14.

<sup>8</sup>Percentages are estimated to the nearest 5% per ASTM D 2488-17.



## SUBSURFACE EXPLORATION PROCEDURE: STANDARD PENETRATION TESTING (SPT) ASTM D 1586 Split-Barrel Sampling

Standard Penetration Testing, or **SPT**, is the most frequently used subsurface exploration test performed worldwide. This test provides samples for identification purposes, as well as a measure of penetration resistance, or N-value. The N-Value, or blow counts, when corrected and correlated, can approximate engineering properties of soils used for geotechnical design and engineering purposes.

### SPT Procedure:

- Involves driving a hollow tube (split-spoon) into the ground by dropping a 140-lb hammer a height of 30-inches at desired depth
- Recording the number of hammer blows required to drive split-spoon a distance of 12 inches (in 3 or 4 Increments of 6 inches each)
- Auger is advanced\* and an additional SPT is performed
- One SPT test is typically performed for every two to five feet
- Obtain two-inch diameter soil sample



*\*Drilling Methods May Vary*— The predominant drilling methods used for SPT are open hole fluid rotary drilling and hollow-stem auger drilling.



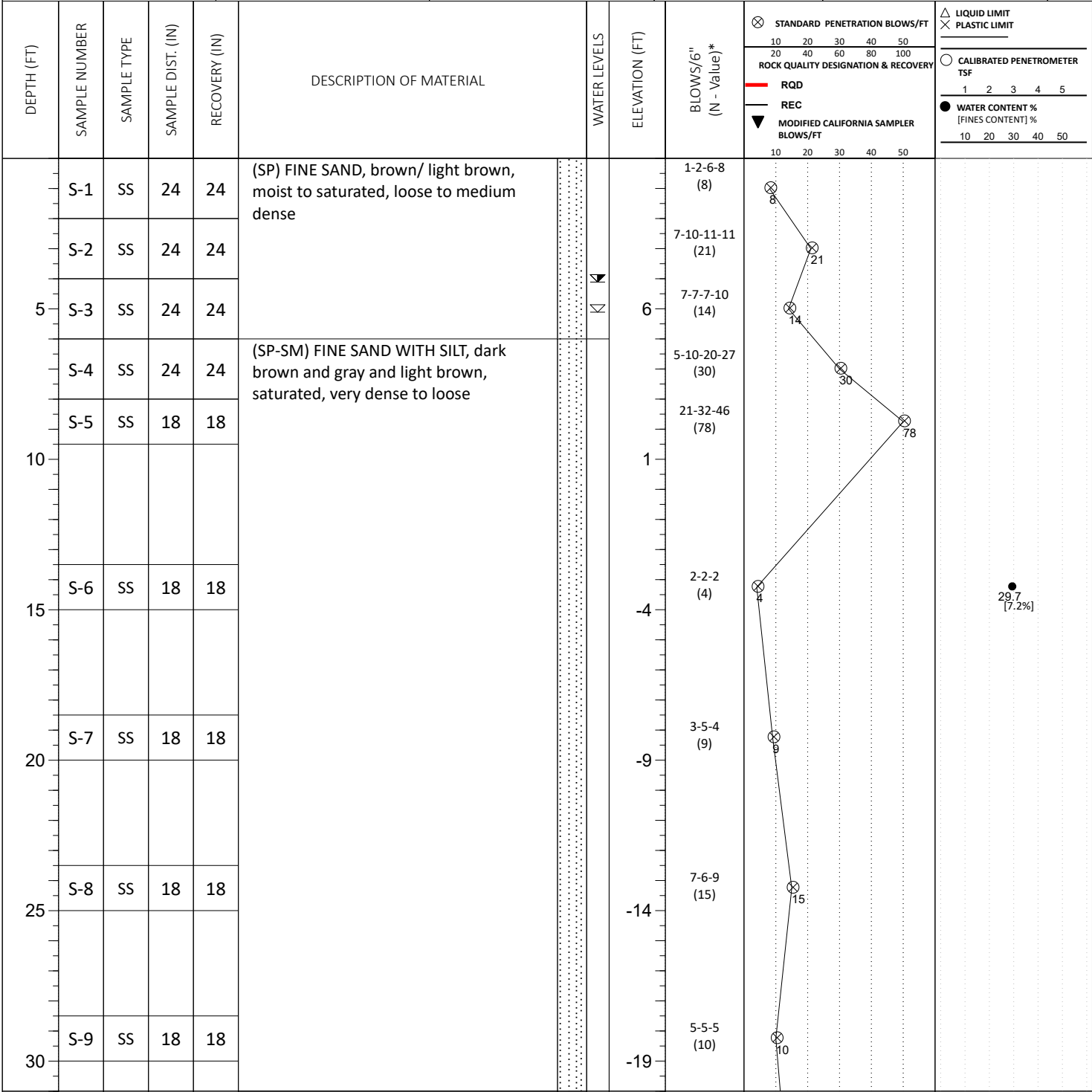
## SUBSURFACE EXPLORATION PROCEDURE: Hand Auger Borings ASTM D1452

In this procedure, a shallow depth boring is made by manually rotating and advancing an auger to the desired depths while periodically removing the auger from the hole to clear and examine the auger cuttings. The auger cuttings are visually classified in the field in accordance with ASTM D2488. Disturbed samples are collected in each soil stratum and sealed in an airtight container and labeled appropriately.

### Hand Auger Procedure:













- Involves manually rotating a tube or barrel type auger to the desired sample depth
- Recording the depth of changes in strata
- Describing soil in each major stratum in accordance with ASTM D2488
- Recording groundwater depth and location of seepage zones, when/if found
- Describing condition of augered hole (i.e. whether the hole remains open or the sides cave)

SITE LOCATION: <b>3550 S. Washington Avenue, Titusville, Florida, 32780</b>			LOSS OF CIRCULATION 	
LATITUDE:	LONGITUDE:	STATION:	SURFACE ELEVATION: <b>11.0</b>	BOTTOM OF CASING 



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THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

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HAMMER TYPE:	<b>Manual - Safety</b>																							
LOGGED BY:	<b>SJ5</b>																							
DRILLING METHOD:																								

**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION: <b>3550 S. Washington Avenue, Titusville, Florida, 32780</b>			LOSS OF CIRCULATION	
LATITUDE:	LONGITUDE:	STATION:	SURFACE ELEVATION: <b>11.0</b>	BOTTOM OF CASING

DEPTH (FT)	SAMPLE NUMBER	SAMPLE TYPE	SAMPLE DIST. (IN)	RECOVERY (IN)	DESCRIPTION OF MATERIAL	WATER LEVELS	ELEVATION (FT)	BLOWS/6" (N - Value)*	STANDARD PENETRATION BLOWS/FT		ROCK QUALITY DESIGNATION & RECOVERY		WATER CONTENT % [FINES CONTENT] %	
									10	20	30	40	50	10
35	S-10	SS	18	18	(SP-SM) FINE SAND WITH SILT, dark brown and gray and light brown, saturated, very dense to loose		-24	7-6-8 (14)	14					
40	S-11	SS	18	18	(SC) CLAYEY FINE SAND, gray, saturated, loose to medium dense		-29	4-3-4 (7)						
45	S-12	SS	18	18			-34	6-7-6 (13)						
50	S-13	SS	18	18			-39	6-7-7 (14)						
55	S-14	SS	18	18	(SC) CLAYEY SAND, gray, saturated, medium dense		-44	3-3-6 (9)						
60	S-15	SS	18	18	(SP-SC) FINE SAND WITH CLAY, contains shell fragments, gray, saturated, medium dense to dense		-49	9-7-13 (20)						

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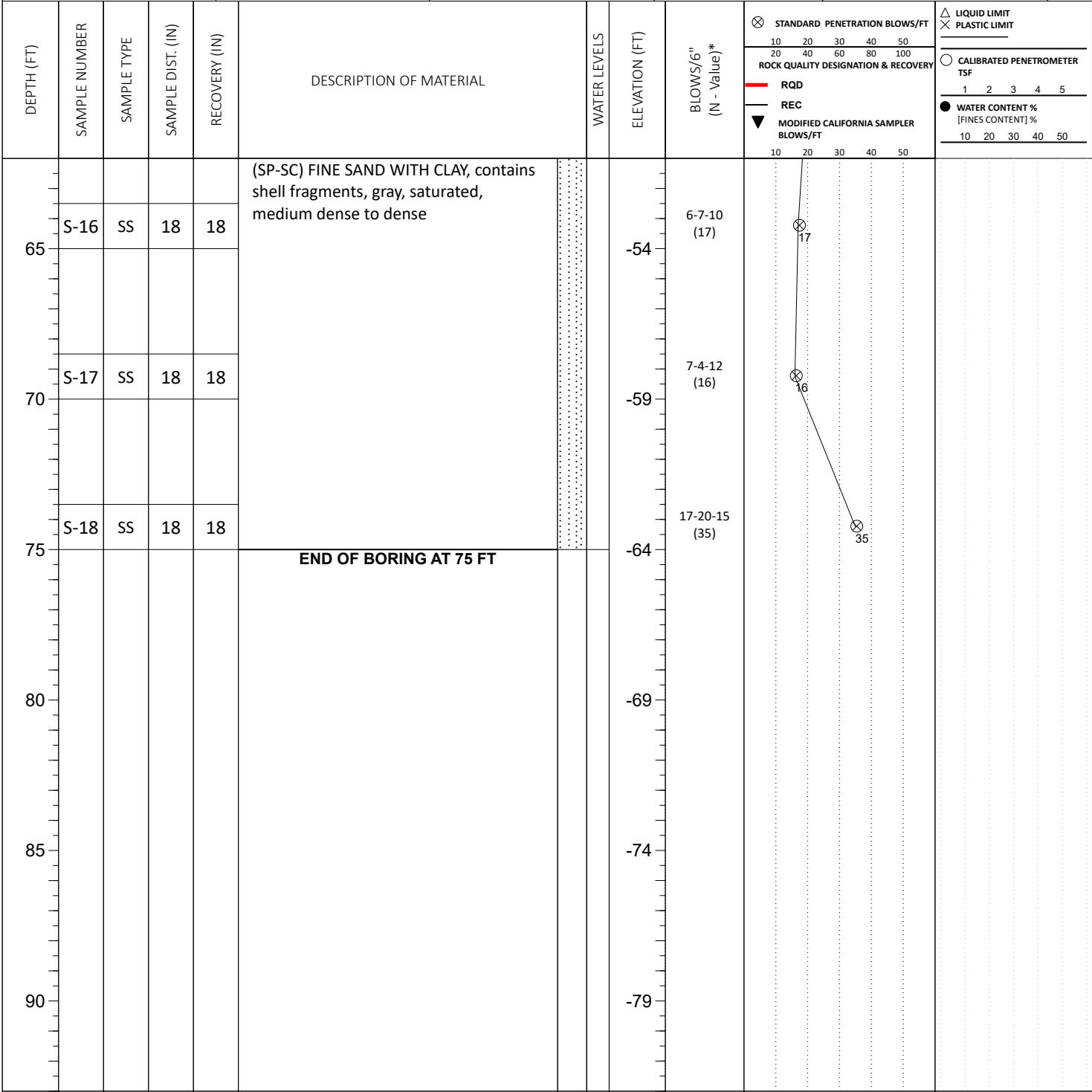
THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

∇ WL (First Encountered) <span style="float: right;"><b>5.00</b></span>	BORING STARTED: <b>Mar 12 2024</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Mar 12 2024</b>	HAMMER TYPE: <b>Manual - Safety</b>
∇ WL (Seasonal High Water) <span style="float: right;"><b>4.00</b></span>	EQUIPMENT: <b>TRACK</b>	LOGGED BY: <b>SJS</b>
∇ WL (Stabilized)		DRILLING METHOD:

**GEOTECHNICAL BOREHOLE LOG**

CLIENT: <b>Titusville Resort and Destination, LLC</b>	PROJECT NO.: <b>56:1380-B</b>	BORING NO.: <b>BF-01</b>	SHEET: <b>3 of 3</b>	
PROJECT NAME: <b>Titusville Mall Redevelopment</b>	DRILLER/CONTRACTOR: <b>Allstate Geotechnical Drilling Inc.</b>			

SITE LOCATION: <b>3550 S. Washington Avenue, Titusville, Florida, 32780</b>			LOSS OF CIRCULATION 	
LATITUDE:	LONGITUDE:	STATION:	SURFACE ELEVATION: <b>11.0</b>	BOTTOM OF CASING 



THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

∇ WL (First Encountered) <b>5.00</b> ▼ WL (Completion) ∇ WL (Seasonal High Water) <b>4.00</b> ∇ WL (Stabilized)	BORING STARTED: <b>Mar 12 2024</b> BORING COMPLETED: <b>Mar 12 2024</b> EQUIPMENT: <b>TRACK</b>	LOGGED BY: <b>SJ5</b>	CAVE IN DEPTH: HAMMER TYPE: <b>Manual - Safety</b> DRILLING METHOD:
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**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION: <b>3550 S. Washington Avenue, Titusville, Florida, 32780</b>			LOSS OF CIRCULATION 
LATITUDE:	LONGITUDE:	STATION:	BOTTOM OF CASING 

DEPTH (FT)	SAMPLE NUMBER	SAMPLE TYPE	SAMPLE D.I.S.T. (IN)	RECOVERY (IN)	DESCRIPTION OF MATERIAL	WATER LEVELS	ELEVATION (FT)	BLOWS/6" (N - Value)*	STANDARD PENETRATION BLOWS/FT		ROCK QUALITY DESIGNATION & RECOVERY		WATER CONTENT % [FINES CONTENT] %		
									10	20	30	40	50	10	20
5	S-1	SS	24	24	(SP) FINE SAND, brown and light brown, moist to saturated, loose to medium dense	▼	2-2-4-8 (6)	6	6	6	6	6			
	S-2	SS	24	24			8-11-14-14 (25)	25							
	S-3	SS	24	24			9-7-11-14 (18)	18							
	S-4	SS	24	24			9-9-13-10 (22)	22							
	S-5	SS	24	24			8-9-9-11 (18)	18							
10					(SP-SC) SAND WITH CLAY, light brown, saturated, medium dense	▼	1								
15	S-6	SS	18	18			6-5-11 (16)	16							
20					(SP) FINE SAND, light brown, saturated, medium dense	▼	-4								
	S-7	SS	18	18			8-9-11 (20)	20							
25	S-8	SS	18	18			5-6-8 (14)	14							
30					(SP-SC) FINE SAND WITH CLAY, gray, saturated, loose to medium dense	▼	-9								
	S-9	SS	18	18			4-6-7 (13)	13							

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THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

▼ WL (First Encountered) <span style="float: right;"><b>5.50</b></span>	BORING STARTED: <b>Mar 12 2024</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Mar 12 2024</b>	HAMMER TYPE: <b>Manual - Safety</b>
▼ WL (Seasonal High Water) <span style="float: right;"><b>4.50</b></span>	EQUIPMENT: <b>TRACK</b>	LOGGED BY: <b>SJ5</b>
▼ WL (Stabilized)		DRILLING METHOD:

**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION: <b>3550 S. Washington Avenue, Titusville, Florida, 32780</b>	LOSS OF CIRCULATION 			
LATITUDE:	LONGITUDE:	STATION:	SURFACE ELEVATION: <b>11.0</b>	BOTTOM OF CASING 

DEPTH (FT)	SAMPLE NUMBER	SAMPLE TYPE	SAMPLE DIST. (IN)	RECOVERY (IN)	DESCRIPTION OF MATERIAL	WATER LEVELS	ELEVATION (FT)	BLOWS/6" (N - Value)*	STANDARD PENETRATION BLOWS/FT		ROCK QUALITY DESIGNATION & RECOVERY		LIQUID LIMIT / PLASTIC LIMIT		CALIBRATED PENETROMETER TSF		WATER CONTENT % [FINES CONTENT] %		
									10	20	30	40	50	10	20	30	40	50	1
35	S-10	SS	18	6	(SP-SC) FINE SAND WITH CLAY, gray, saturated, loose to medium dense		-24	9-11-17 (28)	28										
40	S-11	SS	18	18			-29	6-5-6 (11)	11										
45	S-12	SS	18	18			-34	6-3-5 (8)	8										
50	S-13	SS	18	18	(SC) CLAYEY FINE SAND, gray, saturated, loose to medium dense		-39	3-4-3 (7)	7										
55	S-14	SS	18	18			-44	5-4-6 (10)	10										
60	S-15	SS	18	18	(SC) CLAYEY FINE SAND, gray, saturated, medium dense to loose		-49	6-6-7 (13)	13										
<b>CONTINUED ON NEXT PAGE</b>																			

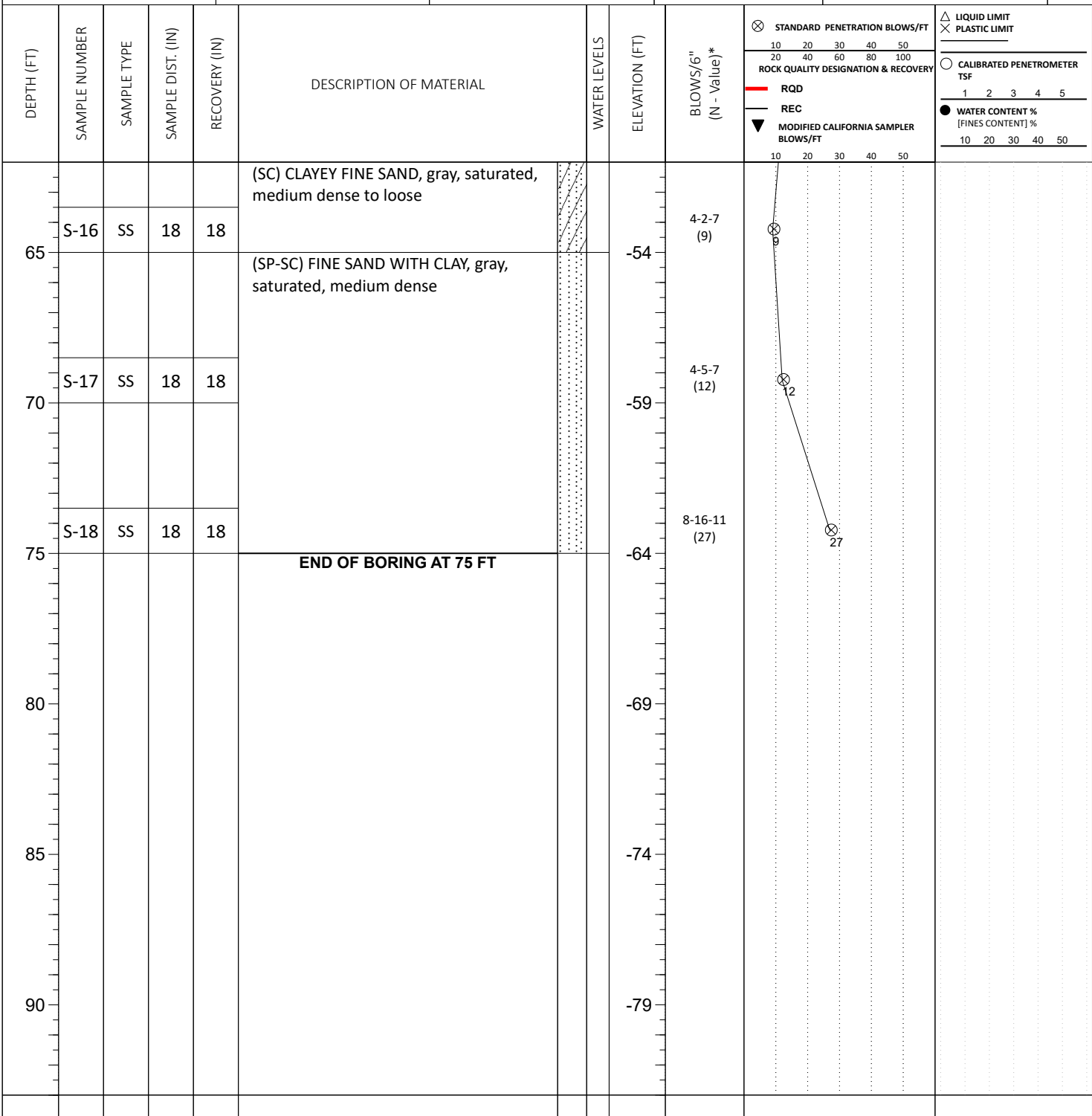
THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

<input checked="" type="checkbox"/> WL (First Encountered) <span style="float: right;"><b>5.50</b></span>	BORING STARTED: <b>Mar 12 2024</b>	CAVE IN DEPTH:
<input checked="" type="checkbox"/> WL (Completion)	BORING COMPLETED: <b>Mar 12 2024</b>	HAMMER TYPE: <b>Manual - Safety</b>
<input checked="" type="checkbox"/> WL (Seasonal High Water) <span style="float: right;"><b>4.50</b></span>	EQUIPMENT: <b>TRACK</b>	LOGGED BY: <b>SJS</b>
<input checked="" type="checkbox"/> WL (Stabilized)		DRILLING METHOD:

### GEOTECHNICAL BOREHOLE LOG

CLIENT: <b>Titusville Resort and Destination, LLC</b>	PROJECT NO.: <b>56:1380-B</b>	BORING NO.: <b>BF-02</b>	SHEET: <b>3 of 3</b>	
PROJECT NAME: <b>Titusville Mall Redevelopment</b>	DRILLER/CONTRACTOR: <b>Allstate Geotechnical Drilling Inc.</b>			

SITE LOCATION: <b>3550 S. Washington Avenue, Titusville, Florida, 32780</b>			LOSS OF CIRCULATION 	
LATITUDE:	LONGITUDE:	STATION:	SURFACE ELEVATION: <b>11.0</b>	BOTTOM OF CASING 

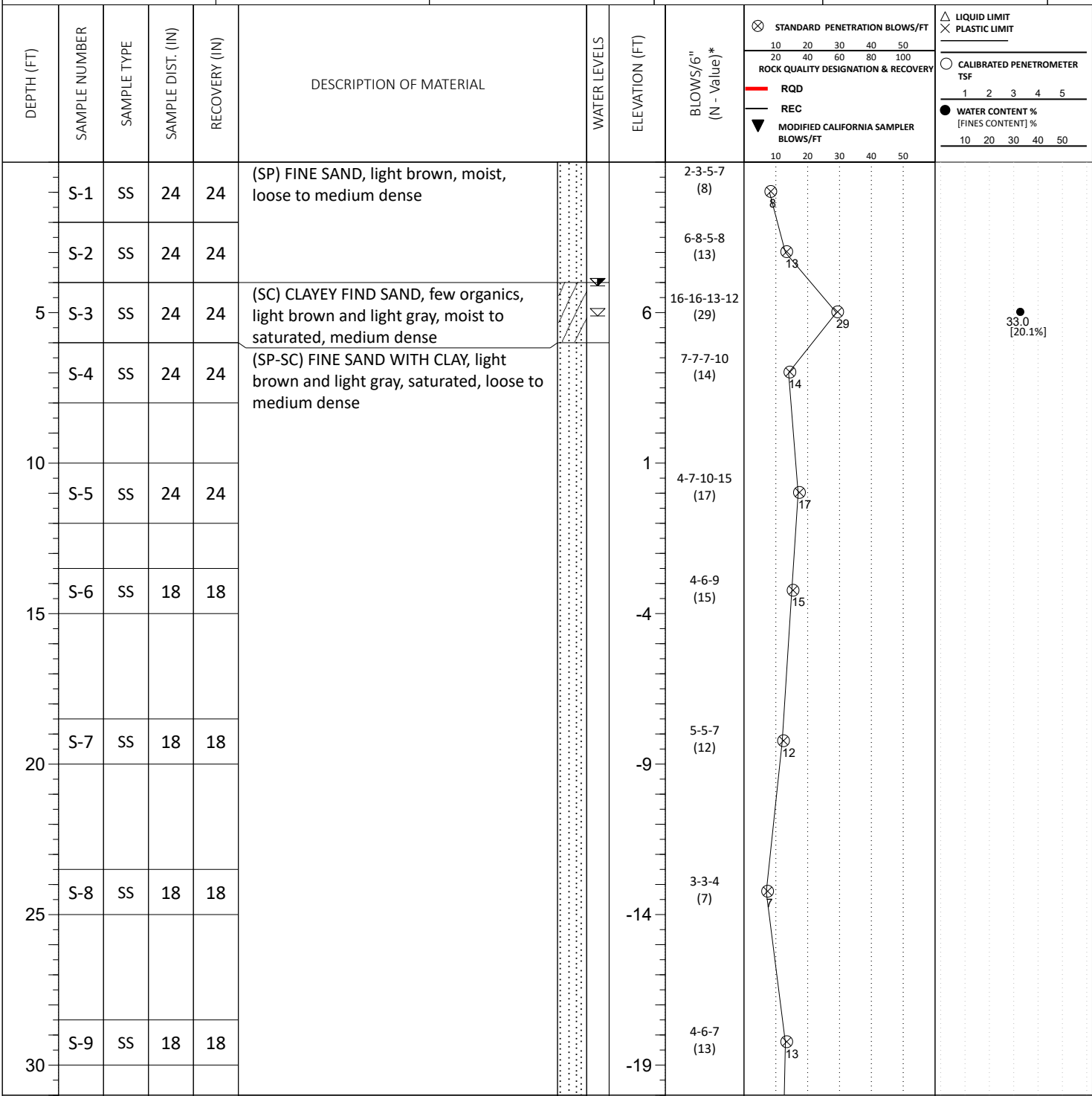


THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

∇ WL (First Encountered) <b>5.50</b> ▼ WL (Completion) ∇ WL (Seasonal High Water) <b>4.50</b> ∇ WL (Stabilized)	BORING STARTED: <b>Mar 12 2024</b> BORING COMPLETED: <b>Mar 12 2024</b> EQUIPMENT: <b>TRACK</b>	LOGGED BY: <b>SJ5</b>	CAVE IN DEPTH: HAMMER TYPE: <b>Manual - Safety</b> DRILLING METHOD:
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**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION: <b>3550 S. Washington Avenue, Titusville, Florida, 32780</b>			LOSS OF CIRCULATION 
LATITUDE:	LONGITUDE:	STATION:	BOTTOM OF CASING 



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THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td>∇ WL (First Encountered)</td> <td style="text-align: center;"><b>5.00</b></td> </tr> <tr> <td>▼ WL (Completion)</td> <td></td> </tr> <tr> <td>∇ WL (Seasonal High Water)</td> <td style="text-align: center;"><b>4.00</b></td> </tr> <tr> <td>∇ WL (Stabilized)</td> <td></td> </tr> </table>	∇ WL (First Encountered)	<b>5.00</b>	▼ WL (Completion)		∇ WL (Seasonal High Water)	<b>4.00</b>	∇ WL (Stabilized)		<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td>BORING STARTED:</td> <td style="text-align: center;"><b>Mar 12 2024</b></td> </tr> <tr> <td>BORING COMPLETED:</td> <td style="text-align: center;"><b>Mar 12 2024</b></td> </tr> <tr> <td>EQUIPMENT:</td> <td style="text-align: center;"><b>TRACK</b></td> </tr> </table>	BORING STARTED:	<b>Mar 12 2024</b>	BORING COMPLETED:	<b>Mar 12 2024</b>	EQUIPMENT:	<b>TRACK</b>	<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td>CAVE IN DEPTH:</td> <td></td> </tr> <tr> <td>HAMMER TYPE:</td> <td style="text-align: center;"><b>Manual - Safety</b></td> </tr> <tr> <td>LOGGED BY:</td> <td style="text-align: center;"><b>SJ5</b></td> </tr> <tr> <td>DRILLING METHOD:</td> <td></td> </tr> </table>	CAVE IN DEPTH:		HAMMER TYPE:	<b>Manual - Safety</b>	LOGGED BY:	<b>SJ5</b>	DRILLING METHOD:	
∇ WL (First Encountered)	<b>5.00</b>																							
▼ WL (Completion)																								
∇ WL (Seasonal High Water)	<b>4.00</b>																							
∇ WL (Stabilized)																								
BORING STARTED:	<b>Mar 12 2024</b>																							
BORING COMPLETED:	<b>Mar 12 2024</b>																							
EQUIPMENT:	<b>TRACK</b>																							
CAVE IN DEPTH:																								
HAMMER TYPE:	<b>Manual - Safety</b>																							
LOGGED BY:	<b>SJ5</b>																							
DRILLING METHOD:																								

**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION: <b>3550 S. Washington Avenue, Titusville, Florida, 32780</b>			LOSS OF CIRCULATION	
LATITUDE:	LONGITUDE:	STATION:	SURFACE ELEVATION: <b>11.0</b>	BOTTOM OF CASING

DEPTH (FT)	SAMPLE NUMBER	SAMPLE TYPE	SAMPLE DIST. (IN)	RECOVERY (IN)	DESCRIPTION OF MATERIAL	WATER LEVELS	ELEVATION (FT)	BLOWS/6" (N - Value)*	STANDARD PENETRATION BLOWS/FT		ROCK QUALITY DESIGNATION & RECOVERY		CALIBRATED PENETROMETER TSF		WATER CONTENT % [FINES CONTENT] %				
									10	20	30	40	50	10	20	30	40	50	1
35	S-10	SS	18	18	(SP-SC) FINE SAND WITH CLAY, light brown and light gray, saturated, loose to medium dense		-24	5-7-5 (12)	⊗	12									
40	S-11	SS	18	18	(SP) FINE SAND, gray, saturated, medium dense, shells		-29	3-2-9 (11)	⊗	11						19.3 [4.8%]			
45	S-12	SS	18	18	(SP-SC) SAND WITH CLAY, contains shell fragments, gray, saturated, medium dense		-34	4-9-7 (16)	⊗	16									
50	S-13	SS	18	18	(SC) CLAYEY SAND, gray, saturated, loose		-39	7-6-5 (11)	⊗	11									
55	S-14	SS	18	18	(SC) CLAYEY SAND, gray, saturated, loose		-44	6-3-4 (7)	⊗	7									
60	S-15	SS	18	18	(SC) CLAYEY SAND, gray, saturated, loose to medium dense		-49	2-3-3 (6)	⊗	6									

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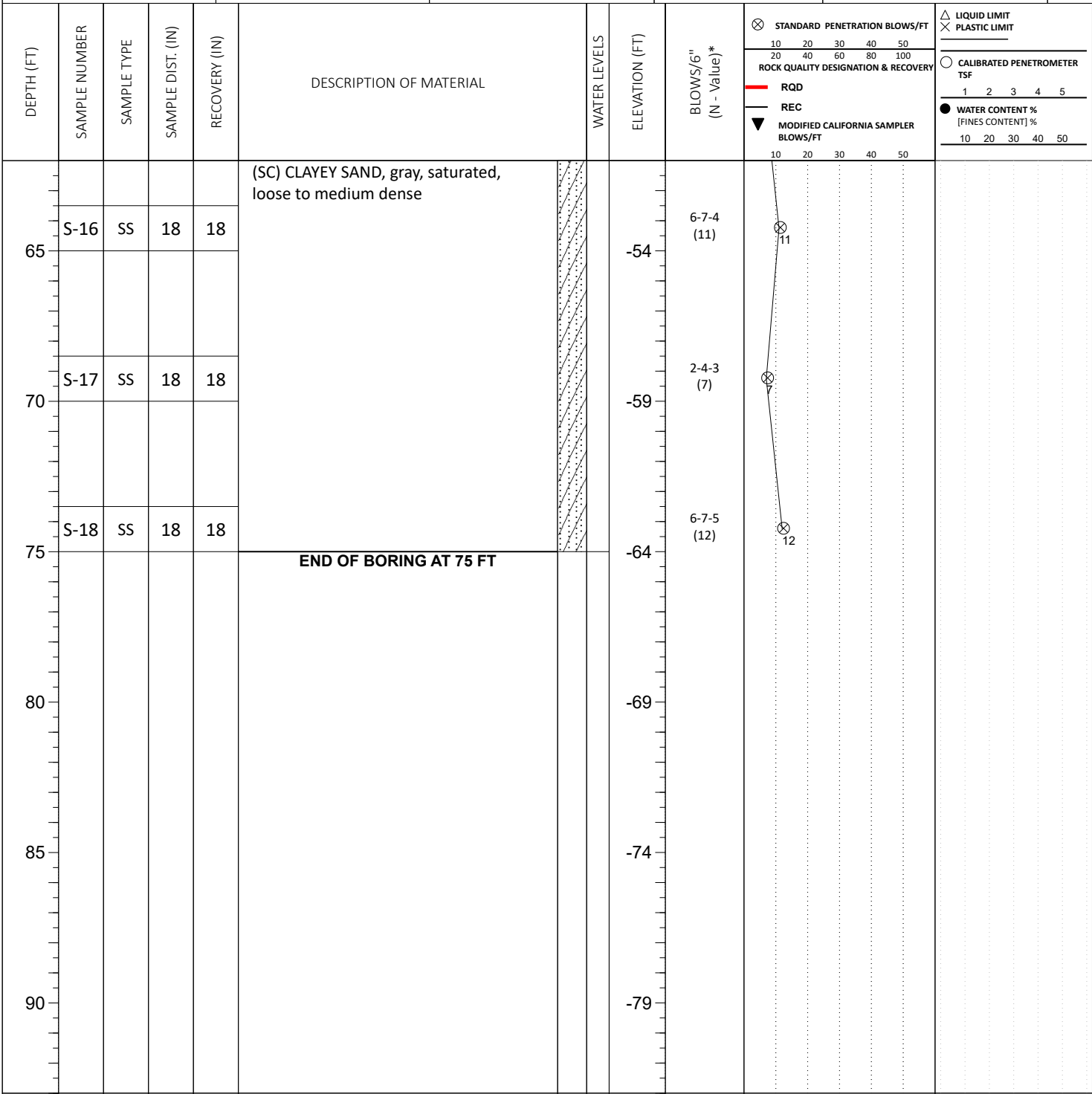
THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

∇ WL (First Encountered) <span style="float: right;"><b>5.00</b></span>	BORING STARTED: <b>Mar 12 2024</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Mar 12 2024</b>	HAMMER TYPE: <b>Manual - Safety</b>
∇ WL (Seasonal High Water) <span style="float: right;"><b>4.00</b></span>	EQUIPMENT: <b>TRACK</b>	LOGGED BY: <b>SJS</b>
∇ WL (Stabilized)		DRILLING METHOD:

**GEOTECHNICAL BOREHOLE LOG**

CLIENT: <b>Titusville Resort and Destination, LLC</b>	PROJECT NO.: <b>56:1380-B</b>	BORING NO.: <b>BF-03</b>	SHEET: <b>3 of 3</b>	
PROJECT NAME: <b>Titusville Mall Redevelopment</b>	DRILLER/CONTRACTOR: <b>Allstate Geotechnical Drilling Inc.</b>			

SITE LOCATION: <b>3550 S. Washington Avenue, Titusville, Florida, 32780</b>			LOSS OF CIRCULATION 	
LATITUDE:	LONGITUDE:	STATION:	SURFACE ELEVATION: <b>11.0</b>	BOTTOM OF CASING 



THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

▽ WL (First Encountered) <span style="float: right;"><b>5.00</b></span>	BORING STARTED: <b>Mar 12 2024</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Mar 12 2024</b>	HAMMER TYPE: <b>Manual - Safety</b>
▽ WL (Seasonal High Water) <span style="float: right;"><b>4.00</b></span>	EQUIPMENT: <b>TRACK</b>	LOGGED BY: <b>SJ5</b>
▽ WL (Stabilized)		DRILLING METHOD:

**GEOTECHNICAL BOREHOLE LOG**


SITE LOCATION: <b>3550 S. Washington Avenue, Titusville, Florida, 32780</b>			LOSS OF CIRCULATION 
LATITUDE:	LONGITUDE:	STATION:	BOTTOM OF CASING 


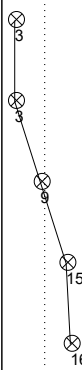

DEPTH (FT)	SAMPLE NUMBER	SAMPLE TYPE	SAMPLE DIST. (IN)	RECOVERY (IN)	DESCRIPTION OF MATERIAL	WATER LEVELS	ELEVATION (FT)	BLOWS/6" (N - Value)*	STANDARD PENETRATION BLOWS/FT		ROCK QUALITY DESIGNATION & RECOVERY		WATER CONTENT % [FINES CONTENT] %	
									10	20	30	40	50	10
5	S-1	SS	24	24	(SP) FINE SAND, light brown, moist to saturated, loose to medium dense			2-2-3-5 (5)						
	S-2	SS	24	24				7-9-13-17 (22)						
	S-3	SS	24	24				7-5-6-6 (11)						
10	S-4	SS	24	24	(SP-SM) FINE SAND WITH SILT, brown, saturated, medium dense			6-7-6-9 (13)						
	S-5	SS	24	24				7-7-7-9 (14)						
15	S-6	SS	18	18				2-3-8 (11)						
					<b>END OF BORING AT 15 FT</b>									

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

▽ WL (First Encountered) <span style="float: right;"><b>6.00</b></span>	BORING STARTED: <b>Mar 13 2024</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Mar 13 2024</b>	HAMMER TYPE: <b>Manual - Safety</b>
▽ WL (Seasonal High Water) <span style="float: right;"><b>5.00</b></span>	EQUIPMENT: <b>TRACK</b>	LOGGED BY: <b>SJ5</b>
▽ WL (Stabilized)		DRILLING METHOD:

### GEOTECHNICAL BOREHOLE LOG


SITE LOCATION: <b>3550 S. Washington Avenue, Titusville, Florida, 32780</b>			LOSS OF CIRCULATION 	
LATITUDE:	LONGITUDE:	STATION:	SURFACE ELEVATION: <b>11.0</b>	BOTTOM OF CASING 


DEPTH (FT)	SAMPLE NUMBER	SAMPLE TYPE	SAMPLE DIST. (IN)	RECOVERY (IN)	DESCRIPTION OF MATERIAL	WATER LEVELS	ELEVATION (FT)	BLOWS/6" (N - Value)*	STANDARD PENETRATION BLOWS/FT		ROCK QUALITY DESIGNATION & RECOVERY		LIQUID LIMIT / PLASTIC LIMIT		CALIBRATED PENETROMETER TSF		WATER CONTENT % [FINES CONTENT] %		
									10	20	30	40	50	10	20	30	40	50	1
5	S-1	SS	24	24	(SP) FINE SAND, brown and light brown, moist to saturated, very loose to loose		1-1-2-4 (3)	13		RQD	REC	MODIFIED CALIFORNIA SAMPLER BLOWS/FT	L	P	CPT	WC			
	S-2	SS	24	24			2-2-1-2 (3)	13											
	S-3	SS	24	24			1-2-7-10 (9)	6											
10	S-4	SS	24	24	(SP-SC) FINE SAND WITH CLAY, brown, saturated, medium dense		5-7-8-7 (15)	15	15	15	15	15	15	15	15	15	15	15	
	S-5	SS	24	24			5-7-9-11 (16)	16											
					<b>END OF BORING AT 10 FT</b>		1												

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td>∇ WL (First Encountered)</td> <td style="text-align: center;"><b>5.00</b></td> </tr> <tr> <td>▼ WL (Completion)</td> <td></td> </tr> <tr> <td>∇ WL (Seasonal High Water)</td> <td style="text-align: center;"><b>4.00</b></td> </tr> <tr> <td>∇ WL (Stabilized)</td> <td></td> </tr> </table>	∇ WL (First Encountered)	<b>5.00</b>	▼ WL (Completion)		∇ WL (Seasonal High Water)	<b>4.00</b>	∇ WL (Stabilized)		<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td>BORING STARTED:</td> <td style="text-align: center;"><b>Mar 14 2024</b></td> </tr> <tr> <td>BORING COMPLETED:</td> <td style="text-align: center;"><b>Mar 14 2024</b></td> </tr> <tr> <td>EQUIPMENT:</td> <td style="text-align: center;"><b>TRACK</b></td> </tr> </table>	BORING STARTED:	<b>Mar 14 2024</b>	BORING COMPLETED:	<b>Mar 14 2024</b>	EQUIPMENT:	<b>TRACK</b>	<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td>CAVE IN DEPTH:</td> <td></td> </tr> <tr> <td>HAMMER TYPE:</td> <td style="text-align: center;"><b>Manual - Safety</b></td> </tr> <tr> <td>LOGGED BY:</td> <td style="text-align: center;"><b>SJ5</b></td> </tr> <tr> <td>DRILLING METHOD:</td> <td></td> </tr> </table>	CAVE IN DEPTH:		HAMMER TYPE:	<b>Manual - Safety</b>	LOGGED BY:	<b>SJ5</b>	DRILLING METHOD:	
∇ WL (First Encountered)	<b>5.00</b>																							
▼ WL (Completion)																								
∇ WL (Seasonal High Water)	<b>4.00</b>																							
∇ WL (Stabilized)																								
BORING STARTED:	<b>Mar 14 2024</b>																							
BORING COMPLETED:	<b>Mar 14 2024</b>																							
EQUIPMENT:	<b>TRACK</b>																							
CAVE IN DEPTH:																								
HAMMER TYPE:	<b>Manual - Safety</b>																							
LOGGED BY:	<b>SJ5</b>																							
DRILLING METHOD:																								

**GEOTECHNICAL BOREHOLE LOG**

CLIENT: <b>Titusville Resort and Destination, LLC</b>	PROJECT NO.: <b>56:1380-B</b>	BORING NO.: <b>BF-06</b>	SHEET: <b>1 of 1</b>	
PROJECT NAME: <b>Titusville Mall Redevelopment</b>	DRILLER/CONTRACTOR: <b>Allstate Geotechnical Drilling Inc.</b>			

SITE LOCATION: <b>3550 S. Washington Avenue, Titusville, Florida, 32780</b>			LOSS OF CIRCULATION	
LATITUDE:	LONGITUDE:	STATION:	SURFACE ELEVATION: <b>11.0</b>	BOTTOM OF CASING

DEPTH (FT)	SAMPLE NUMBER	SAMPLE TYPE	SAMPLE DIST. (IN)	RECOVERY (IN)	DESCRIPTION OF MATERIAL	WATER LEVELS	ELEVATION (FT)	BLOWS/6" (N - Value)*	STANDARD PENETRATION BLOWS/FT		ROCK QUALITY DESIGNATION & RECOVERY		CALIBRATED PENETROMETER TSF		WATER CONTENT % [FINES CONTENT] %		
									10	20	30	40	50	10	20	30	40
2-1-4-8 (5)	S-1	SS	24	24	(SP) FINE SAND, light brown and brown, moist to saturated, loose to medium dense			5									
8-12-15-16 (27)	S-2	SS	24	24	(SP-SM) FINE SAND WITH SILT, brown and dark brown, saturated, medium dense			27									
11-12-15-21 (27)	S-3	SS	24	24				27									
5-6-12-11 (18)	S-4	SS	24	24	(SP) SAND, brown and dark brown, saturated, medium dense			18									
9-12-17-19 (29)	S-5	SS	24	24				29									
<b>END OF BORING AT 10 FT</b>																	

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

∇ WL (First Encountered) <b>6.00</b>	BORING STARTED: <b>Mar 14 2024</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Mar 14 2024</b>	HAMMER TYPE: <b>Manual - Safety</b>
∇ WL (Seasonal High Water) <b>5.00</b>	EQUIPMENT: <b>TRACK</b>	LOGGED BY: <b>SJS</b>
∇ WL (Stabilized)		DRILLING METHOD:

**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION: <b>3550 S. Washington Avenue, Titusville, Florida, 32780</b>	LOSS OF CIRCULATION	100%
LATITUDE:	LONGITUDE:	STATION:
SURFACE ELEVATION: <b>11.0</b>		
BOTTOM OF CASING		▶

DEPTH (FT)	SAMPLE NUMBER	SAMPLE TYPE	SAMPLE DIST. (IN)	RECOVERY (IN)	DESCRIPTION OF MATERIAL	WATER LEVELS	ELEVATION (FT)	BLOWS/6" (N - Value)*	STANDARD PENETRATION BLOWS/FT		ROCK QUALITY DESIGNATION & RECOVERY		LIQUID LIMIT / PLASTIC LIMIT		CALIBRATED PENETROMETER TSF		WATER CONTENT % [FINES CONTENT] %			
									10	20	30	40	50	10	20	30	40	50	1	2
1-2	S-1	SS	24	24	(SP) FINE SAND, dark brown, moist, loose		6	(6)	6											
6-6	S-2	SS	24	24	(SP) SAND, light brown and brown, moist, medium dense		6	(13)	13											
5-4	S-3	SS	24	24	(SP-SM) SAND WITH SILT, light to dark brown, moist to saturated, medium dense		6	(12)	12											
5-6	S-4	SS	24	24			6	(13)	13											
9-13	S-5	SS	24	24			6	(26)	26											
<b>END OF BORING AT 10 FT</b>																				

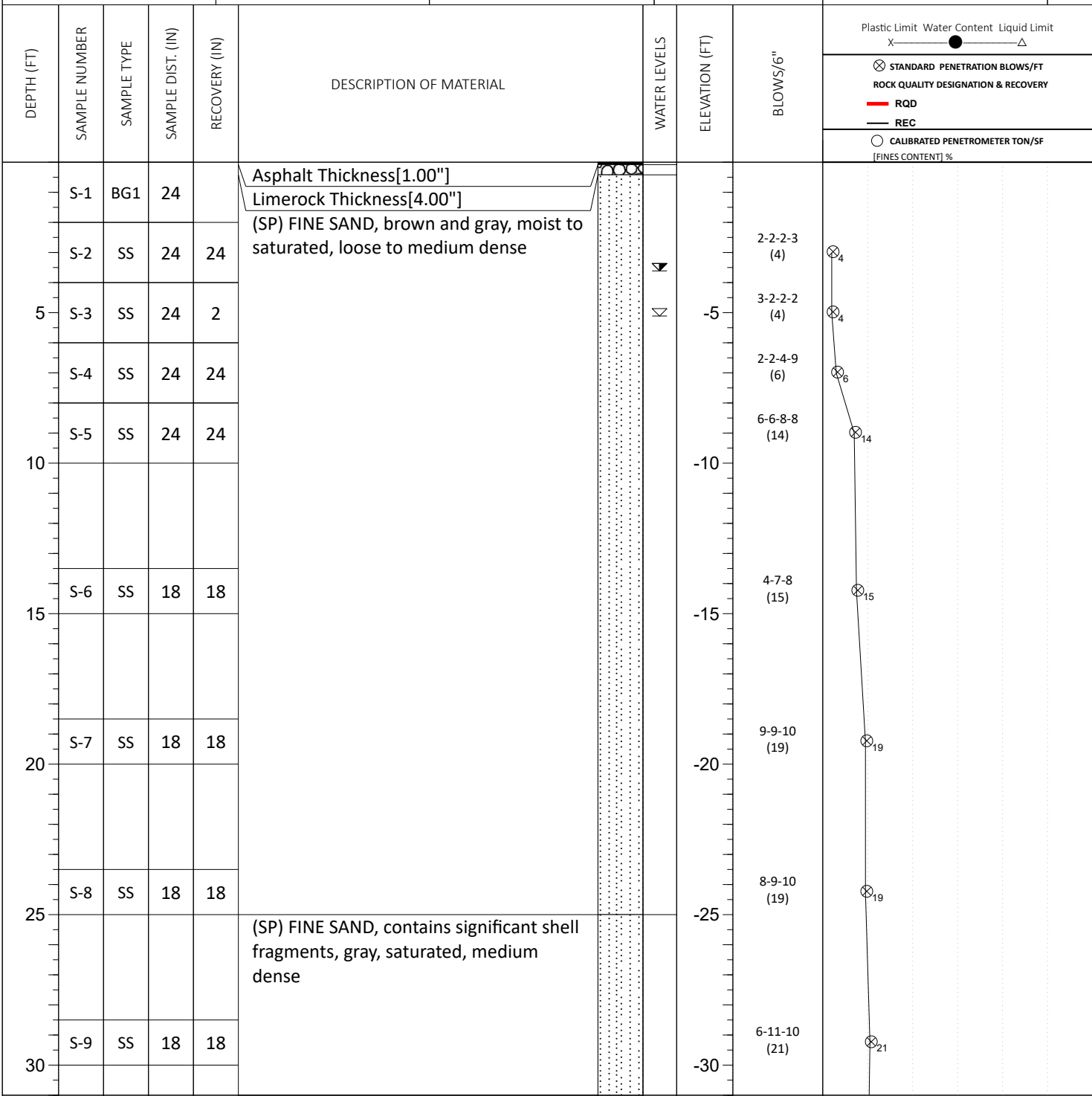
THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

∇ WL (First Encountered) <span style="float: right;"><b>5.00</b></span>	BORING STARTED: <b>Mar 14 2024</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Mar 14 2024</b>	HAMMER TYPE: <b>Manual - Safety</b>
∇ WL (Seasonal High Water) <span style="float: right;"><b>4.00</b></span>	EQUIPMENT: <b>TRACK</b>	LOGGED BY: <b>SJ5</b>
∇ WL (Stabilized)		DRILLING METHOD:

**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION:  
**3550 S Washington Avenue, Titusville, Florida 32780**

NORTHING:	EASTING:	STATION:	SURFACE ELEVATION:	LOSS OF CIRCULATION
				BOTTOM OF CASING



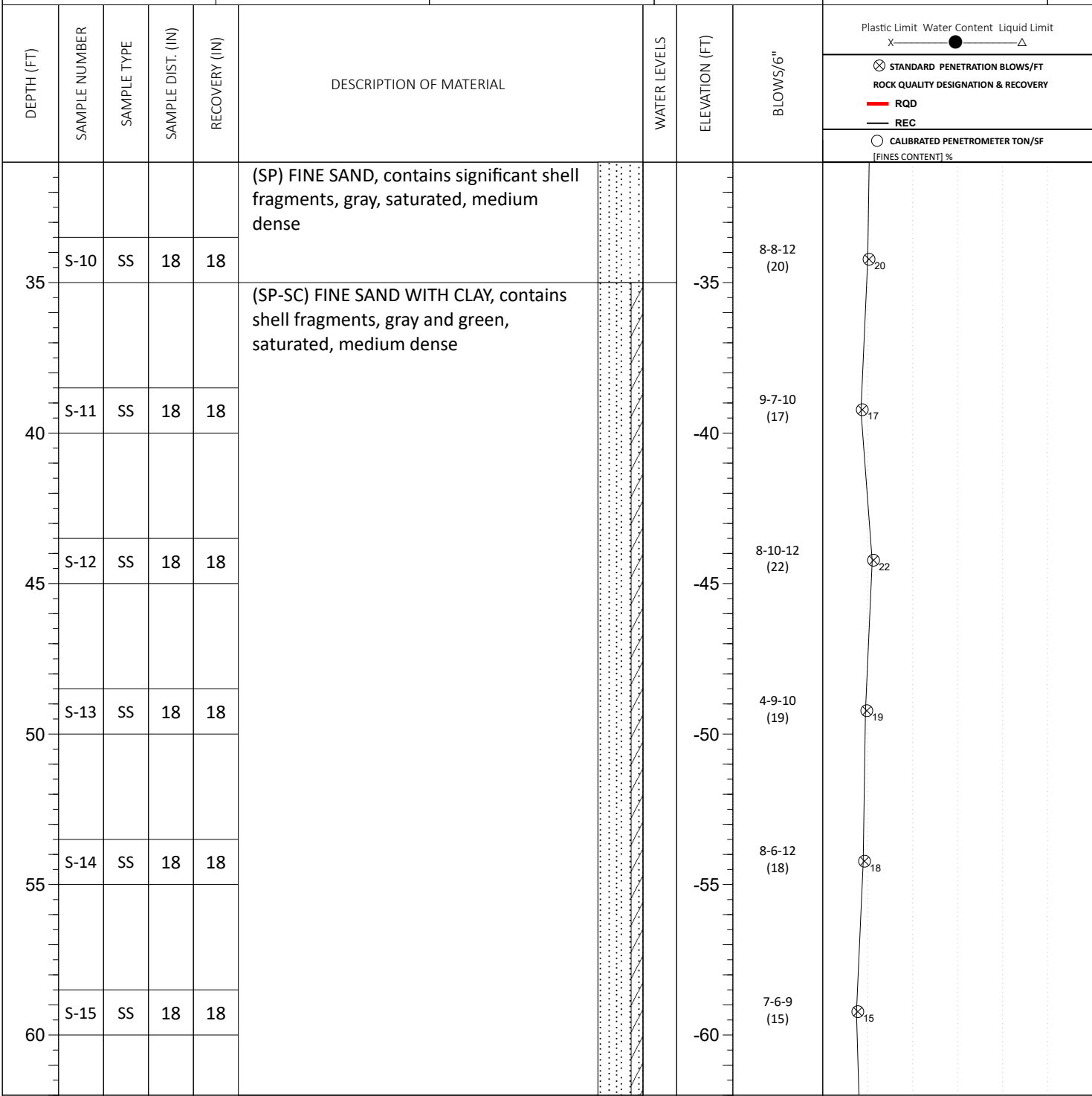
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THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

∇ WL (First Encountered) <span style="float: right;"><b>5.00</b></span>	BORING STARTED: <b>Dec 01 2021</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Dec 01 2021</b>	HAMMER TYPE: <b>Manual</b>
∇ WL (Seasonal High Water) <span style="float: right;"><b>3.50</b></span>	EQUIPMENT: <b>Track</b>	LOGGED BY: <b>VA1</b>
∇ WL (Stabilized)		DRILLING METHOD: <b>Mud-Rotary</b>

**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION: <b>3550 S Washington Avenue, Titusville, Florida 32780</b>			LOSS OF CIRCULATION 
NORTHING:	EASTING:	STATION:	BOTTOM OF CASING 





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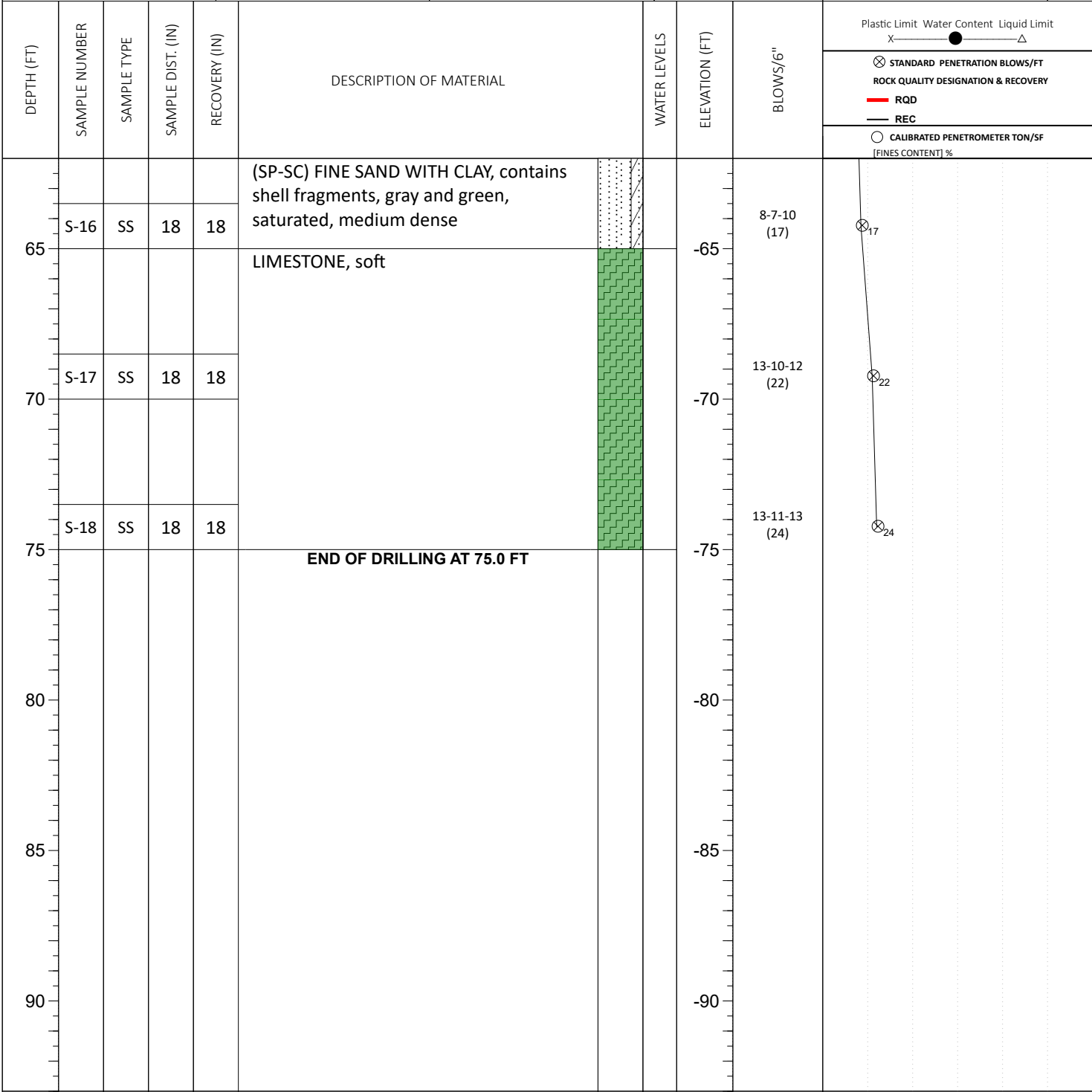
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▽ WL (Seasonal High Water) <span style="float: right;"><b>3.50</b></span>	EQUIPMENT: <b>Track</b>	DRILLING METHOD: <b>Mud-Rotary</b>
▾ WL (Stabilized)	LOGGED BY: <b>VA1</b>	

**GEOTECHNICAL BOREHOLE LOG**

CLIENT: <b>California Retail Properties Corp.</b>	PROJECT NO.: <b>56:1380-A</b>	BORING NO.: <b>B-01</b>	SHEET: <b>3 of 3</b>	
PROJECT NAME: <b>Titusville Resort &amp; Destination</b>	DRILLER/CONTRACTOR: <b>Allstate Geotechnical Drilling Inc.</b>			

SITE LOCATION: <b>3550 S Washington Avenue, Titusville, Florida 32780</b>			LOSS OF CIRCULATION	
NORTHING:	EASTING:	STATION:	SURFACE ELEVATION:	BOTTOM OF CASING



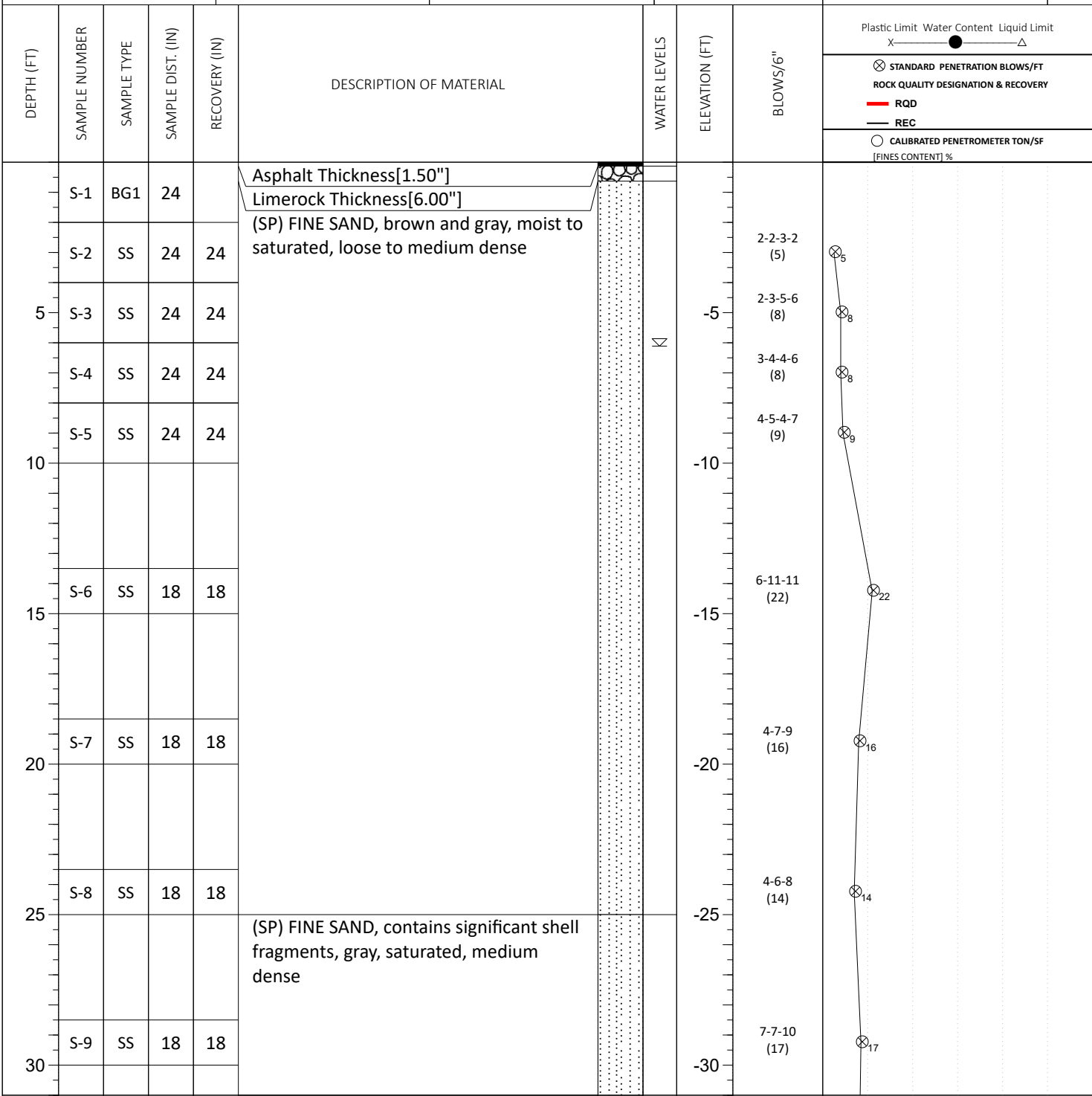
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∇ WL (Seasonal High Water)	<b>3.50</b>	EQUIPMENT:	<b>Track</b>	LOGGED BY:
∇ WL (Stabilized)			<b>VA1</b>	DRILLING METHOD: <b>Mud-Rotary</b>

**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION:  
**3550 S Washington Avenue, Titusville, Florida 32780**

NORTHING:	EASTING:	STATION:	SURFACE ELEVATION:	LOSS OF CIRCULATION
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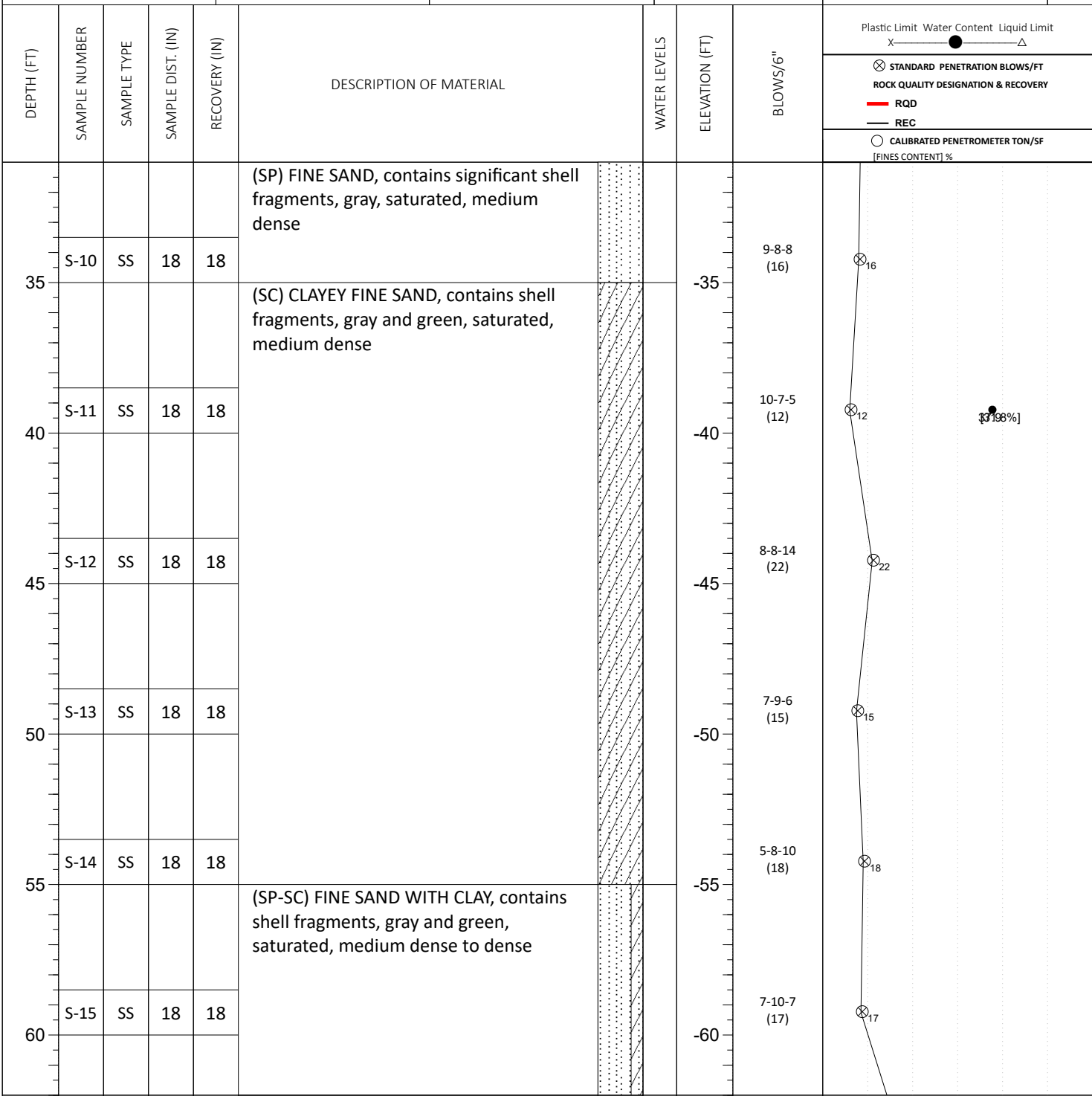
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THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

☒ WL (First Encountered)	<b>6.00</b>	BORING STARTED:	<b>Nov 30 2021</b>	CAVE IN DEPTH:
▼ WL (Completion)		BORING COMPLETED:	<b>Nov 30 2021</b>	HAMMER TYPE: <b>Manual</b>
☒ WL (Seasonal High Water)		EQUIPMENT:	<b>Track</b>	LOGGED BY:
☒ WL (Stabilized)			<b>VA1</b>	DRILLING METHOD: <b>Mud-Rotary</b>

**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION: <b>3550 S Washington Avenue, Titusville, Florida 32780</b>	LOSS OF CIRCULATION	
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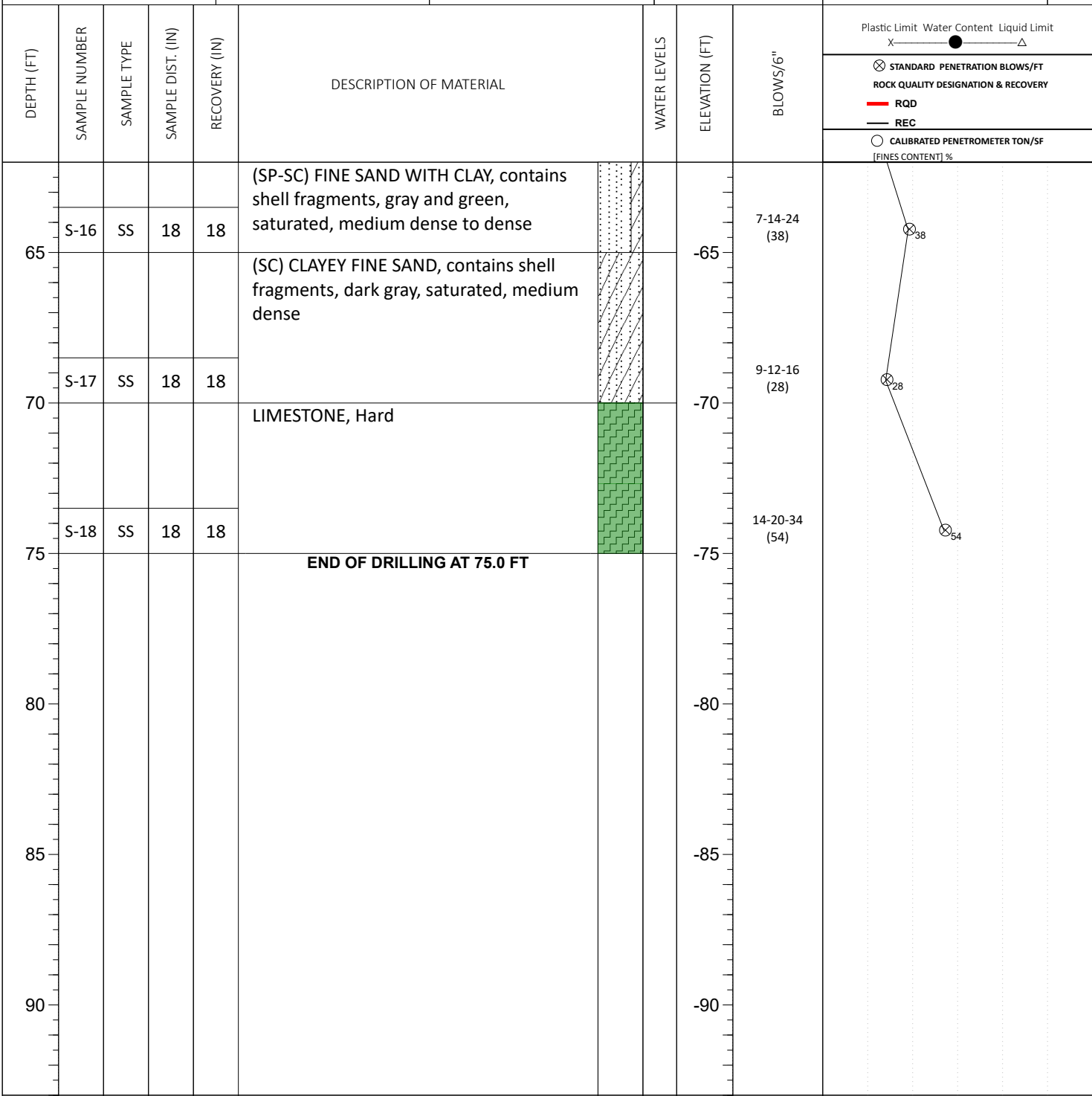
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<input checked="" type="checkbox"/> WL (Seasonal High Water)	EQUIPMENT: <b>Track</b>	DRILLING METHOD: <b>Mud-Rotary</b>
<input checked="" type="checkbox"/> WL (Stabilized)	LOGGED BY: <b>VA1</b>	

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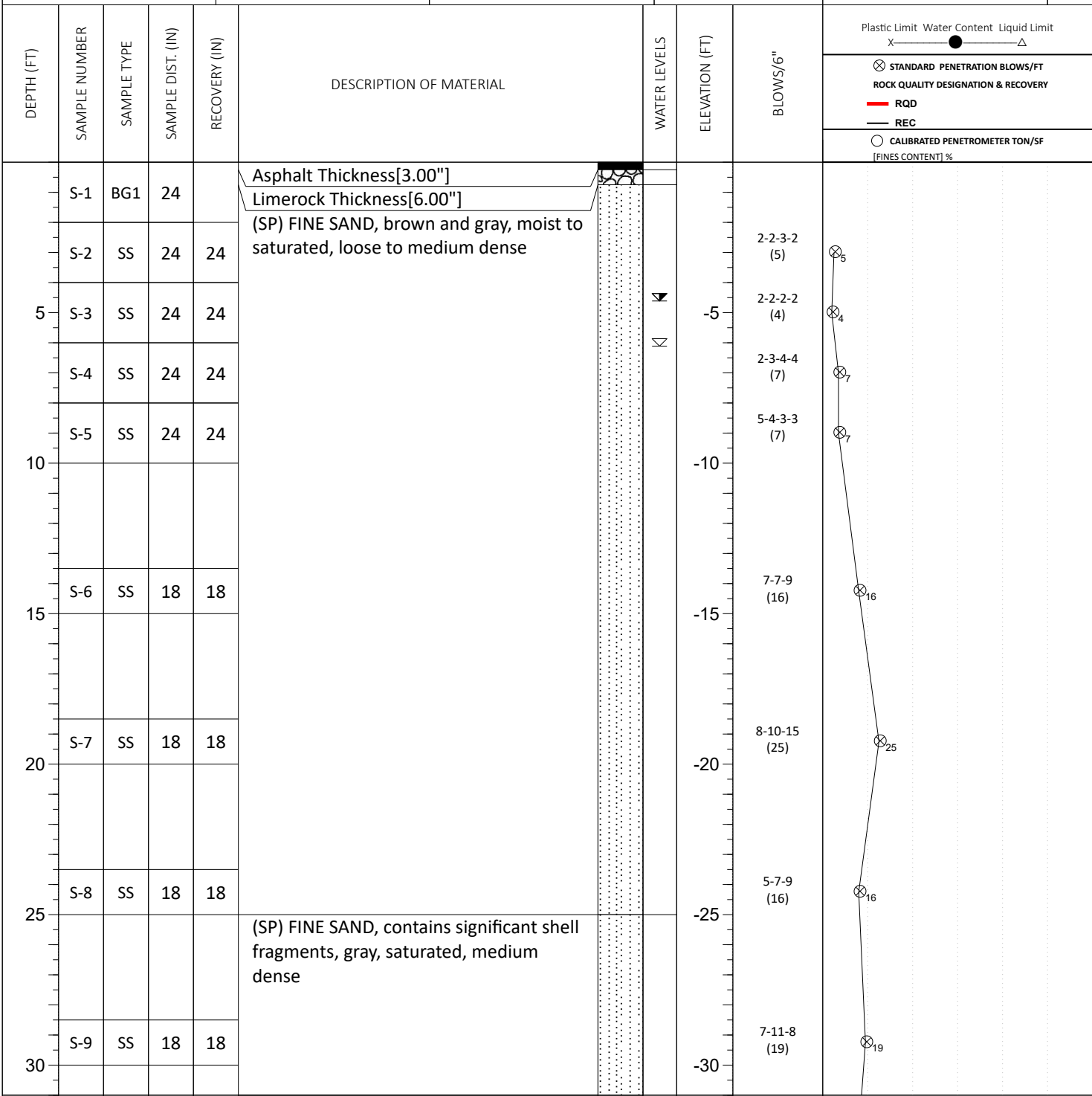
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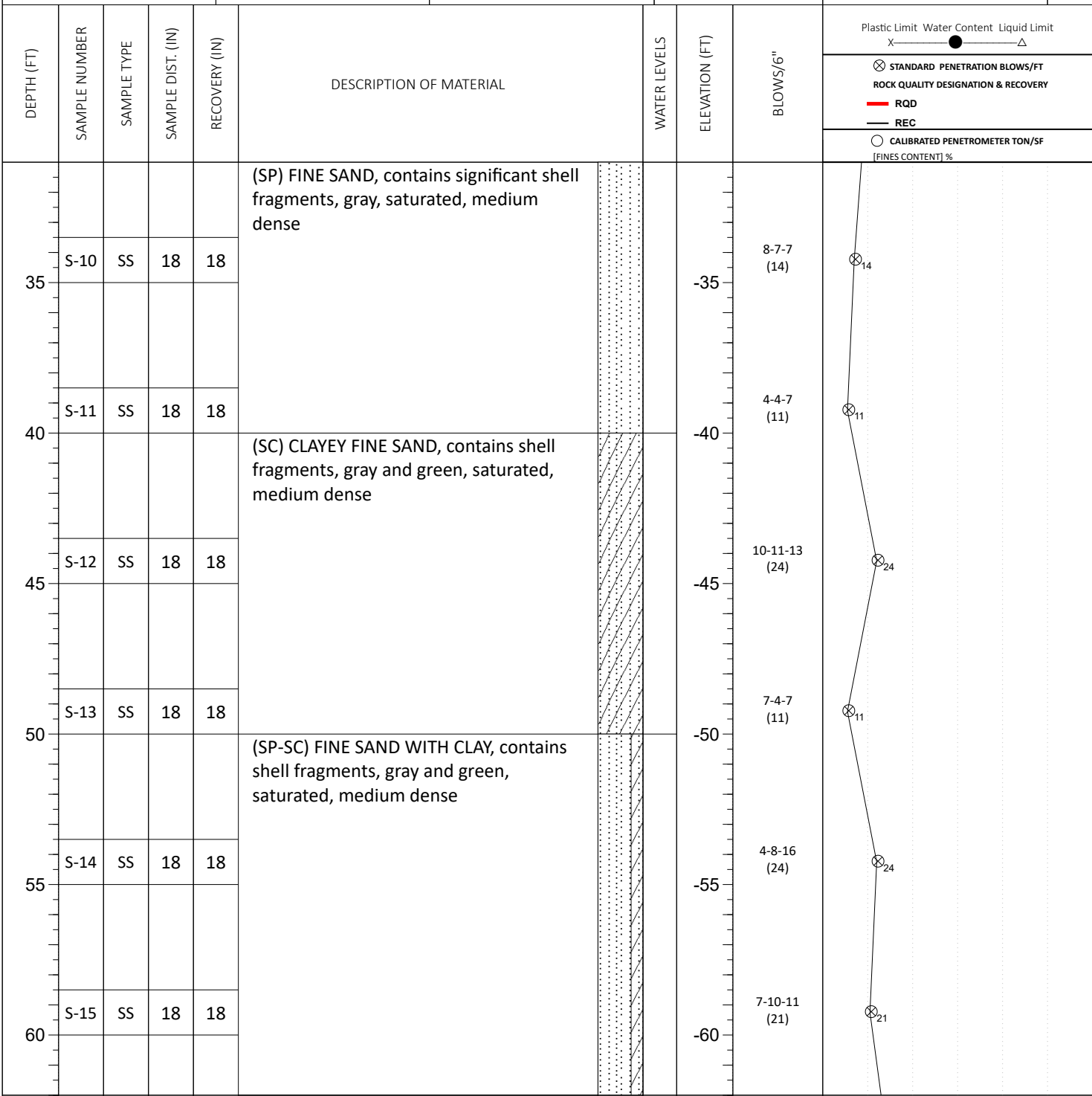
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◊ WL (Seasonal High Water) <span style="float: right;"><b>4.50</b></span>	EQUIPMENT: <b>Track</b>	LOGGED BY: <b>VA1</b>
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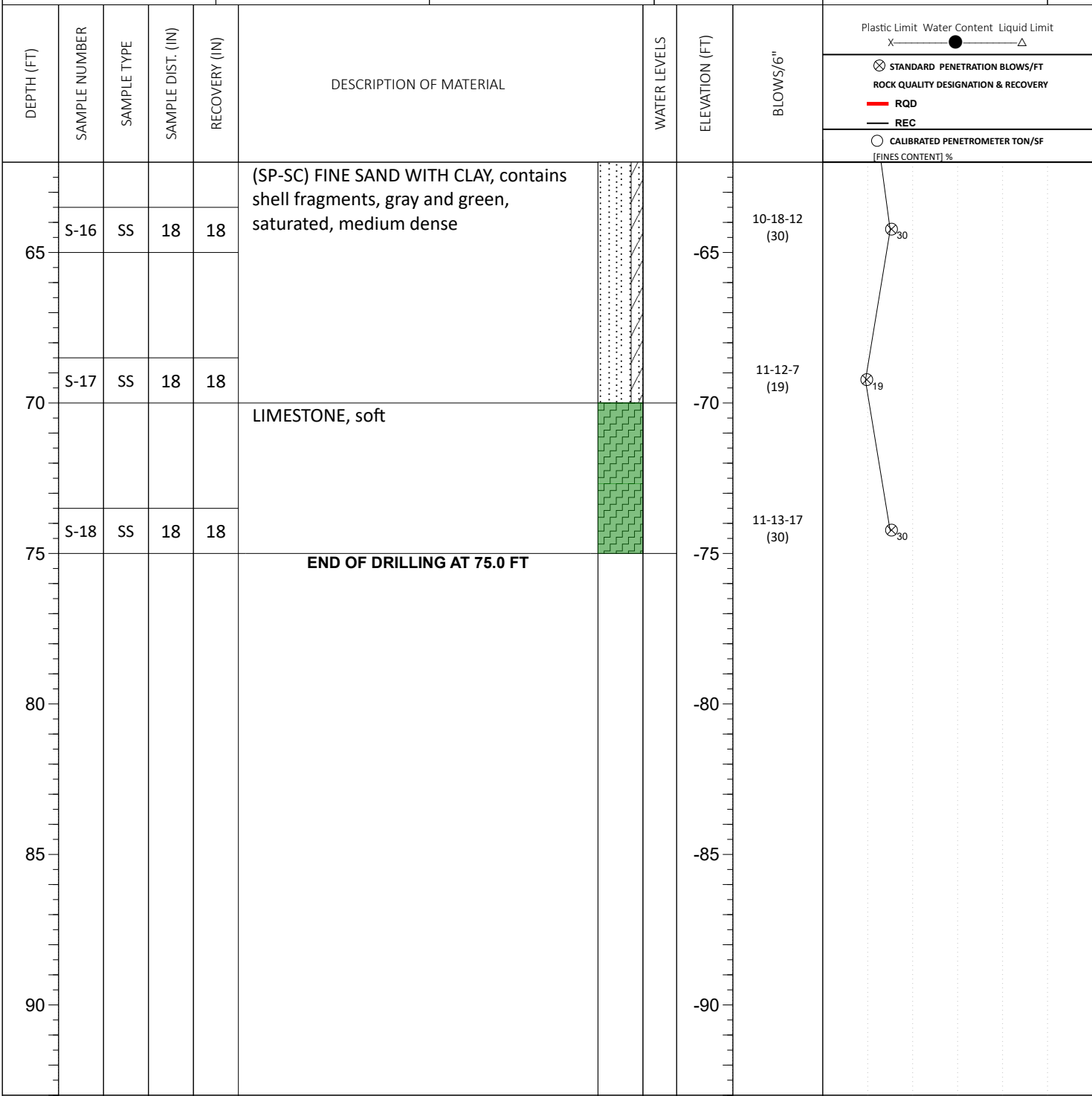
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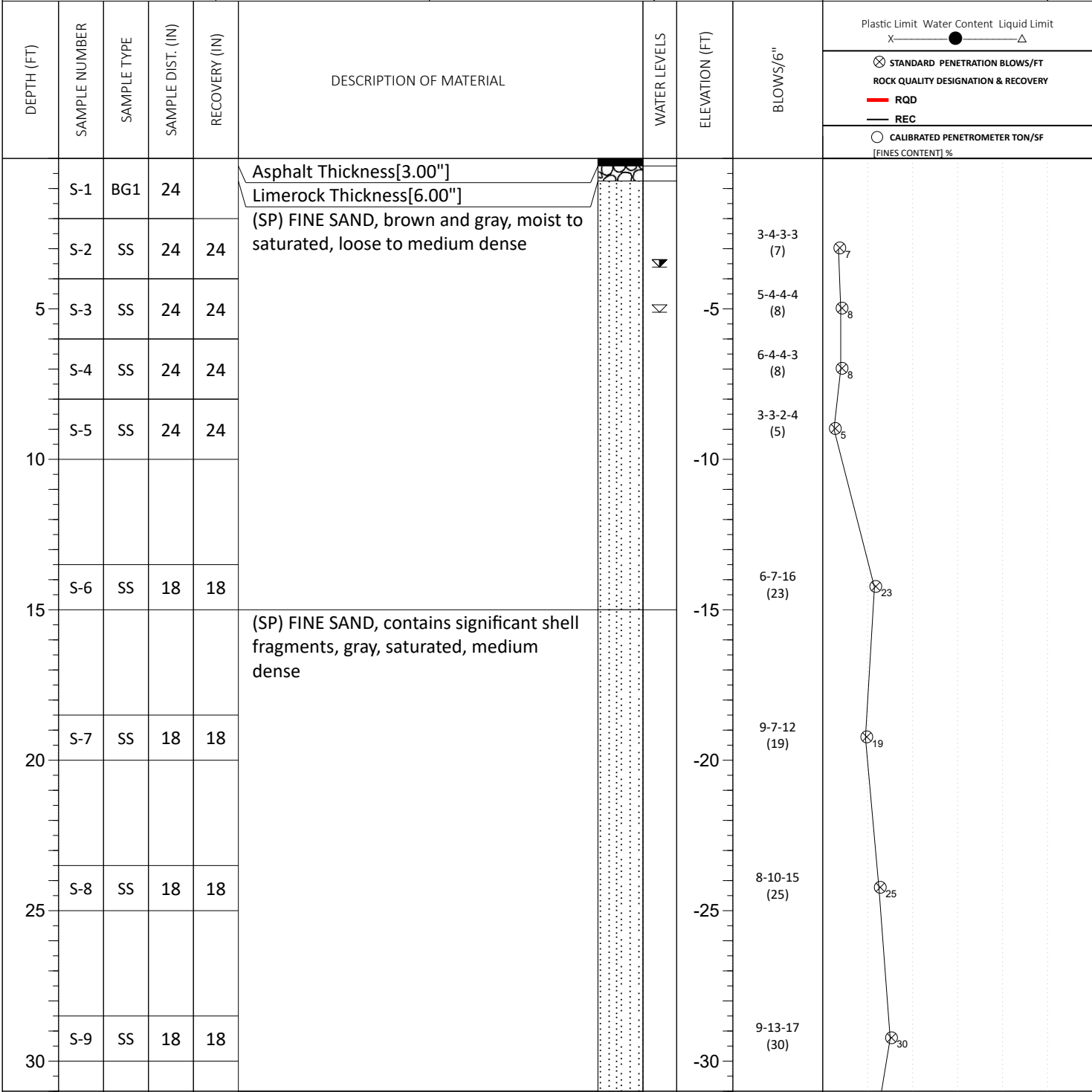


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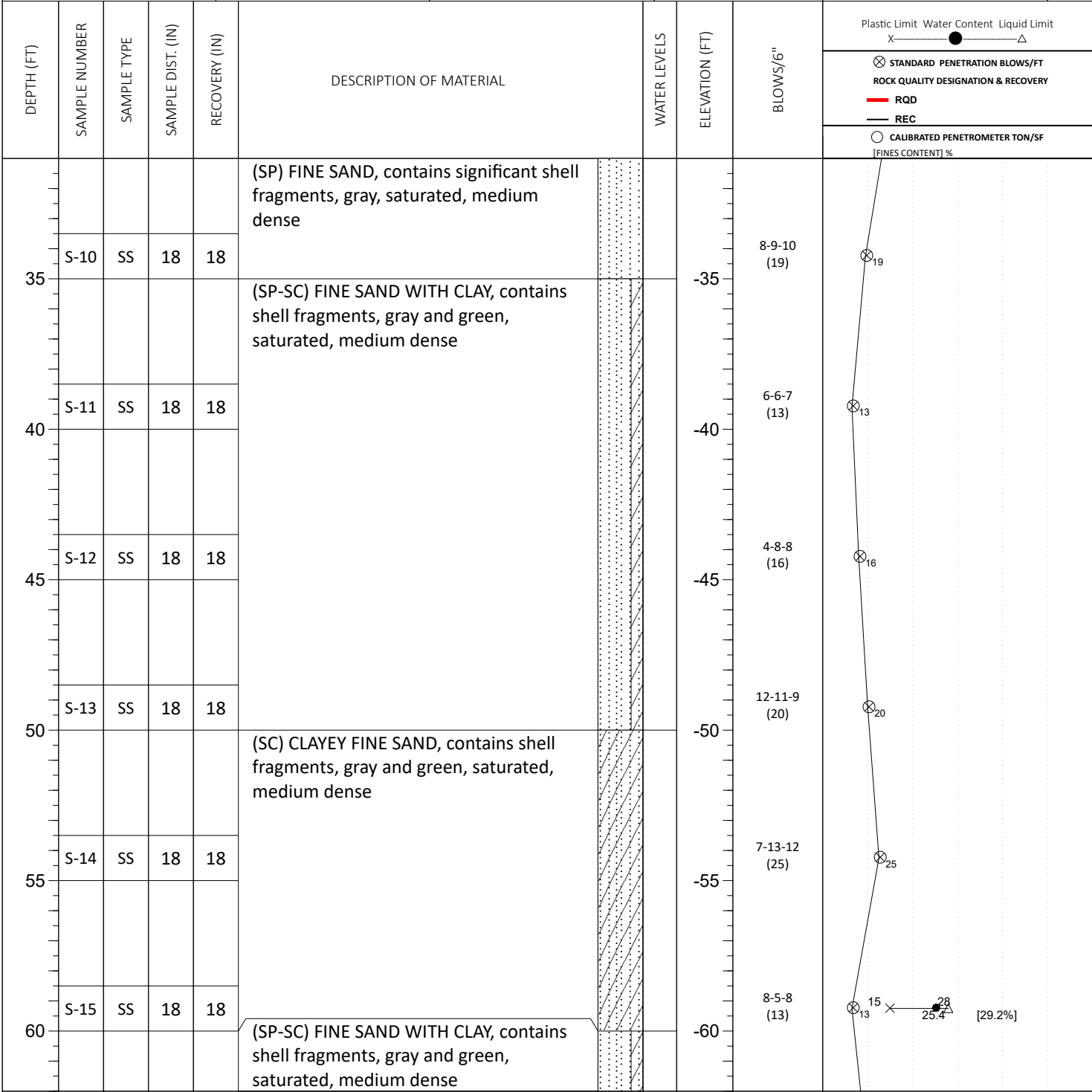
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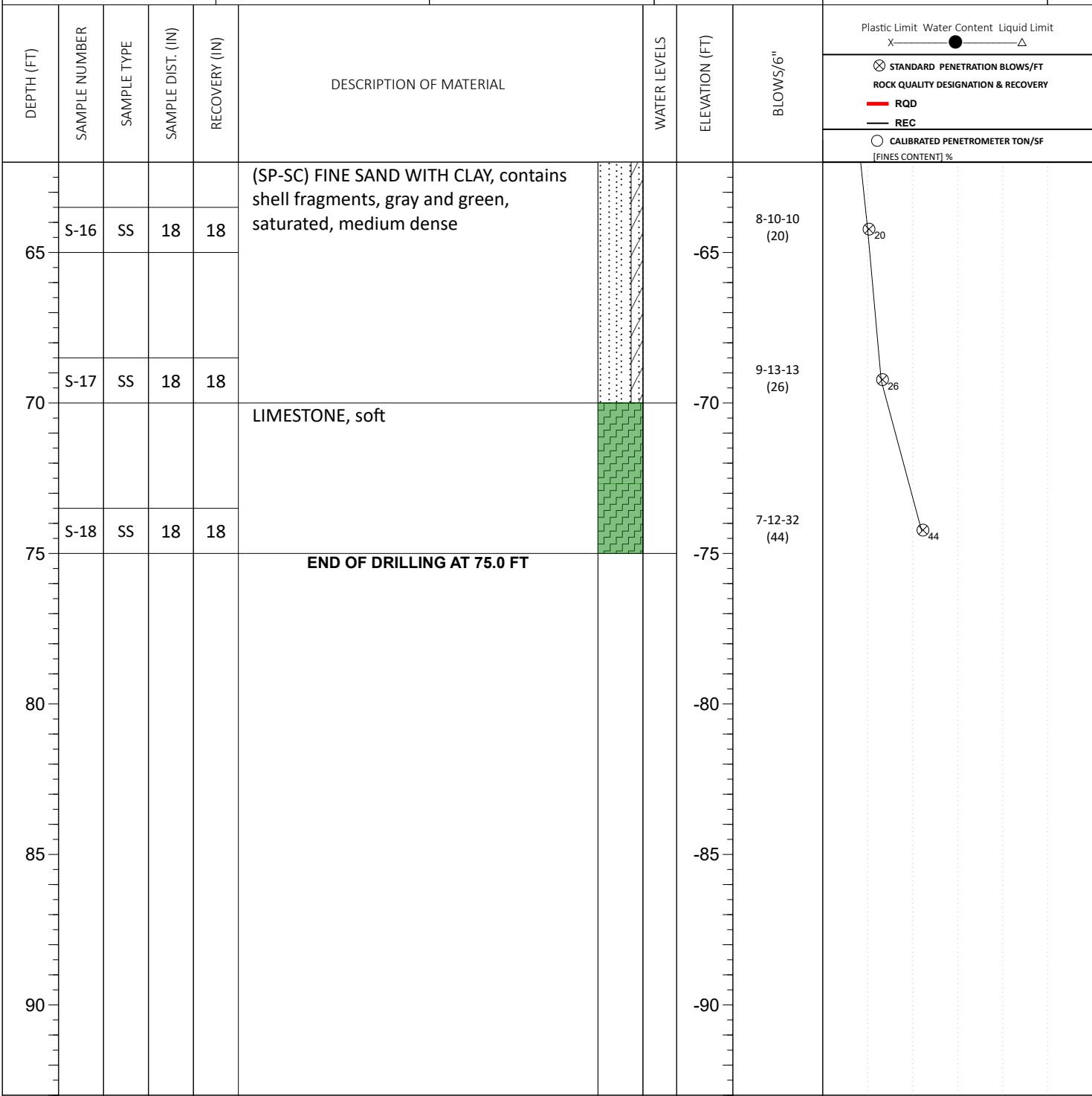
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NORTHING:	EASTING:	STATION:	SURFACE ELEVATION:	BOTTOM OF CASING



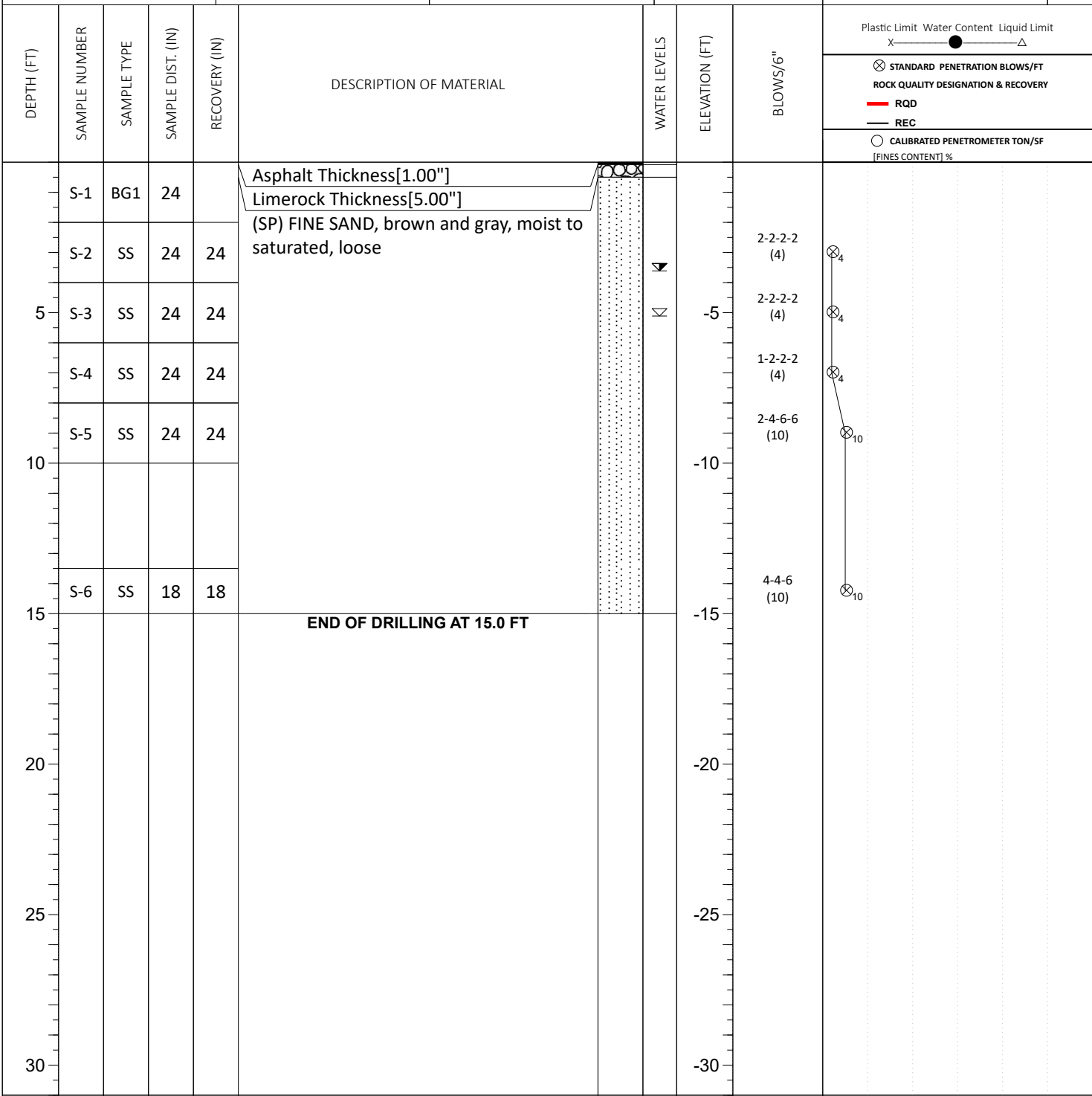
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**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION:  
**3550 S Washington Avenue, Titusville, Florida 32780**

NORTHING:	EASTING:	STATION:	SURFACE ELEVATION:	LOSS OF CIRCULATION
				BOTTOM OF CASING



Plastic Limit Water Content Liquid Limit  
X ● ———— Δ

STANDARD PENETRATION BLOWS/FT  
ROCK QUALITY DESIGNATION & RECOVERY

— RQD  
— REC

CALIBRATED PENETROMETER TON/SF  
[FINES CONTENT] %

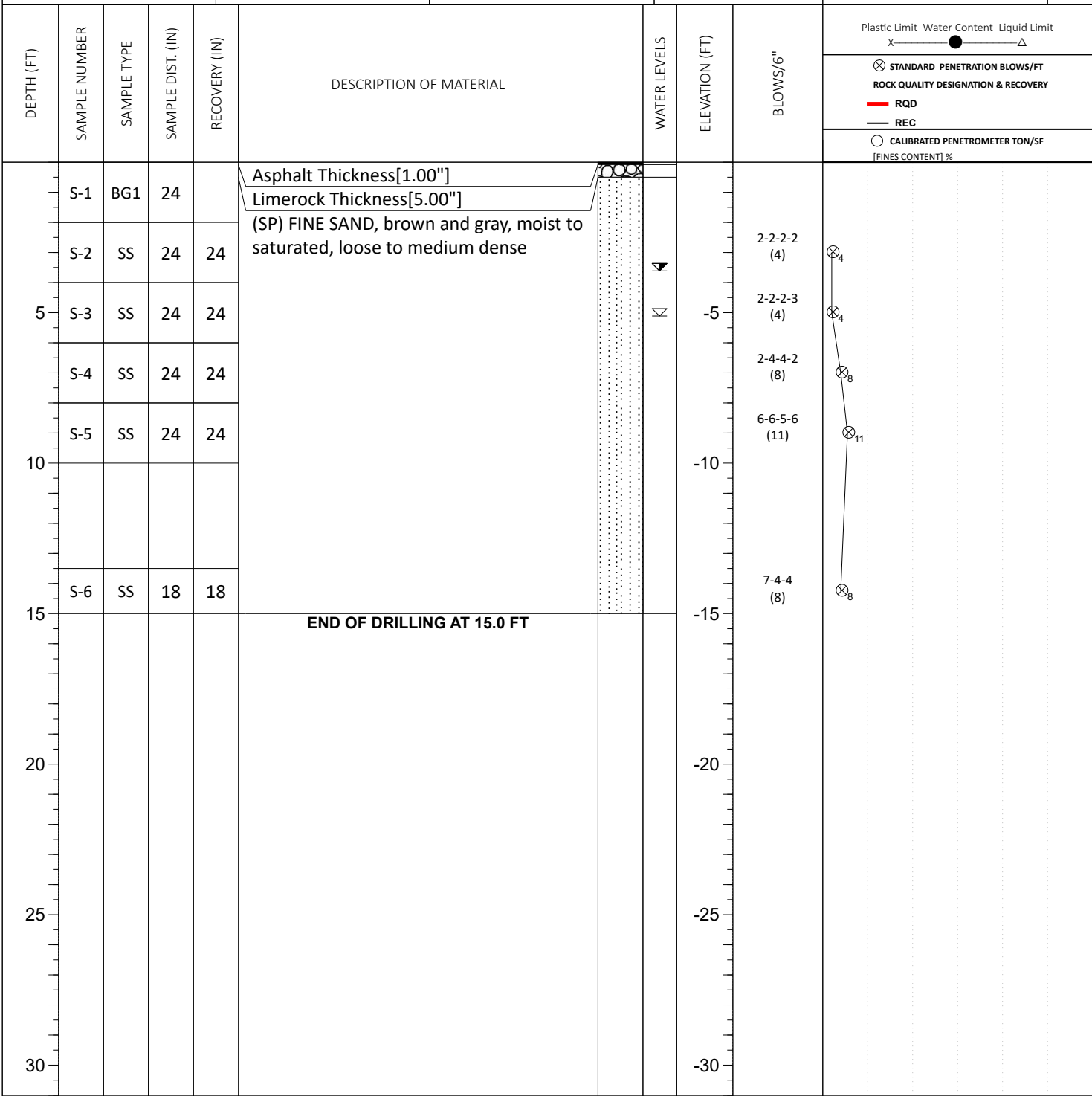
THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td style="width:50%;">∇ WL (First Encountered)</td> <td style="width:10%; text-align: center;"><b>5.00</b></td> </tr> <tr> <td>▼ WL (Completion)</td> <td></td> </tr> <tr> <td>∇ WL (Seasonal High Water)</td> <td style="text-align: center;"><b>3.50</b></td> </tr> <tr> <td>∇ WL (Stabilized)</td> <td></td> </tr> </table>	∇ WL (First Encountered)	<b>5.00</b>	▼ WL (Completion)		∇ WL (Seasonal High Water)	<b>3.50</b>	∇ WL (Stabilized)		<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td>BORING STARTED:</td> <td style="text-align: center;"><b>Dec 01 2021</b></td> </tr> <tr> <td>BORING COMPLETED:</td> <td style="text-align: center;"><b>Dec 01 2021</b></td> </tr> <tr> <td>EQUIPMENT: Track</td> <td>LOGGED BY: VA1</td> </tr> </table>	BORING STARTED:	<b>Dec 01 2021</b>	BORING COMPLETED:	<b>Dec 01 2021</b>	EQUIPMENT: Track	LOGGED BY: VA1	<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td>CAVE IN DEPTH:</td> <td></td> </tr> <tr> <td>HAMMER TYPE:</td> <td style="text-align: center;"><b>Auto</b></td> </tr> <tr> <td>DRILLING METHOD:</td> <td style="text-align: center;"><b>Mud-Rotary</b></td> </tr> </table>	CAVE IN DEPTH:		HAMMER TYPE:	<b>Auto</b>	DRILLING METHOD:	<b>Mud-Rotary</b>
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**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION:  
**3550 S Washington Avenue, Titusville, Florida 32780**

NORTHING:	EASTING:	STATION:	SURFACE ELEVATION:	LOSS OF CIRCULATION 
				BOTTOM OF CASING 



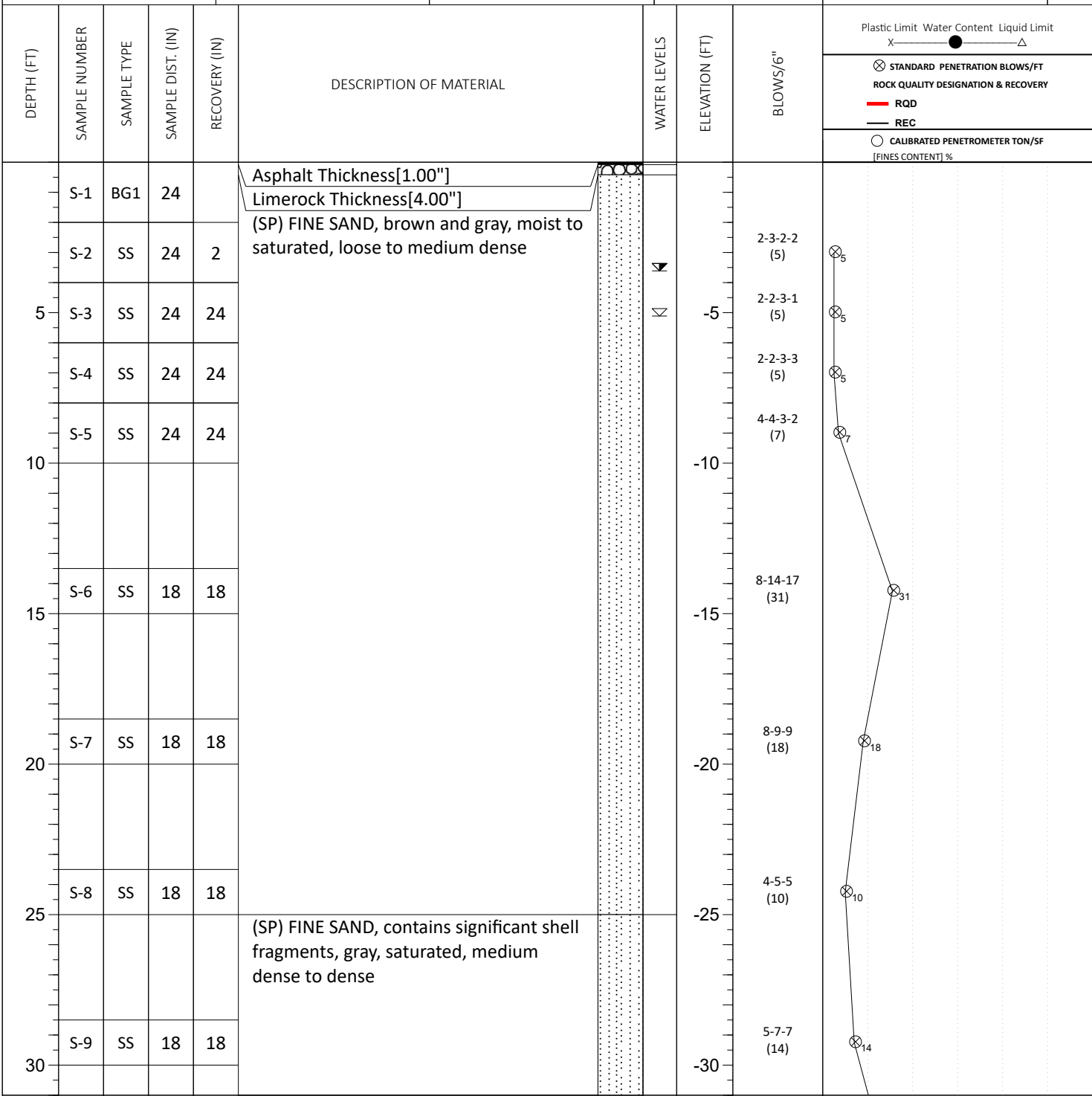
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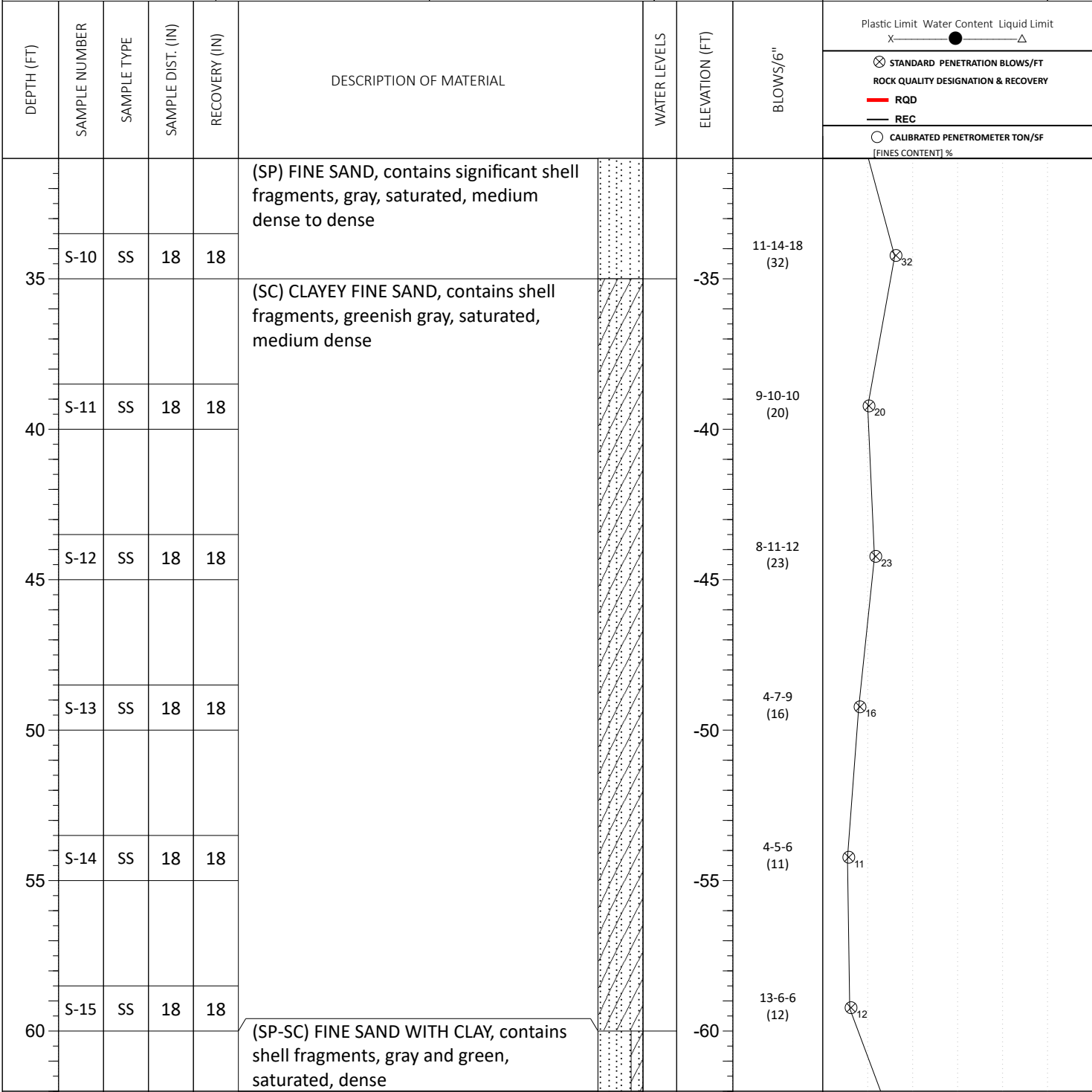
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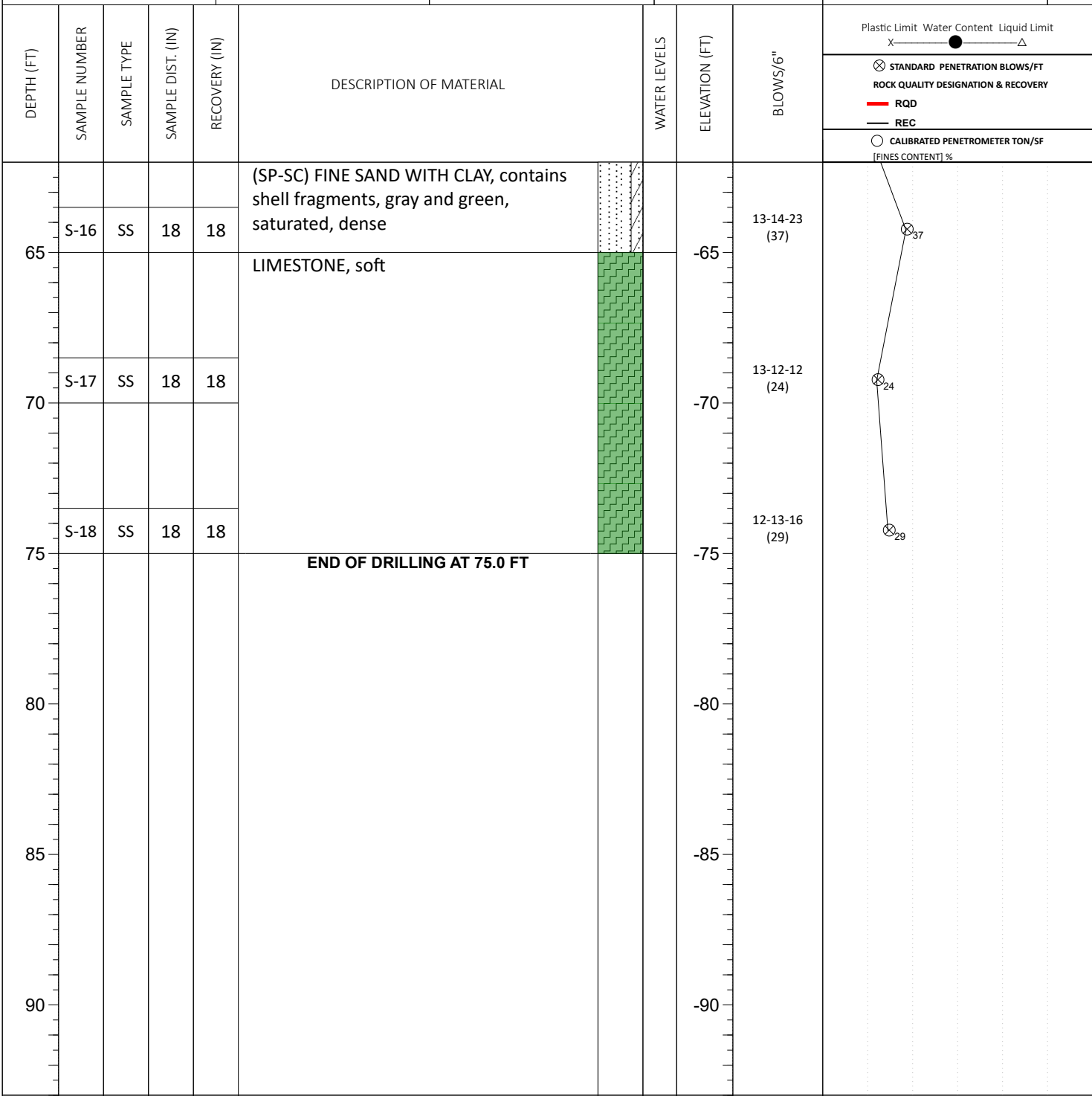
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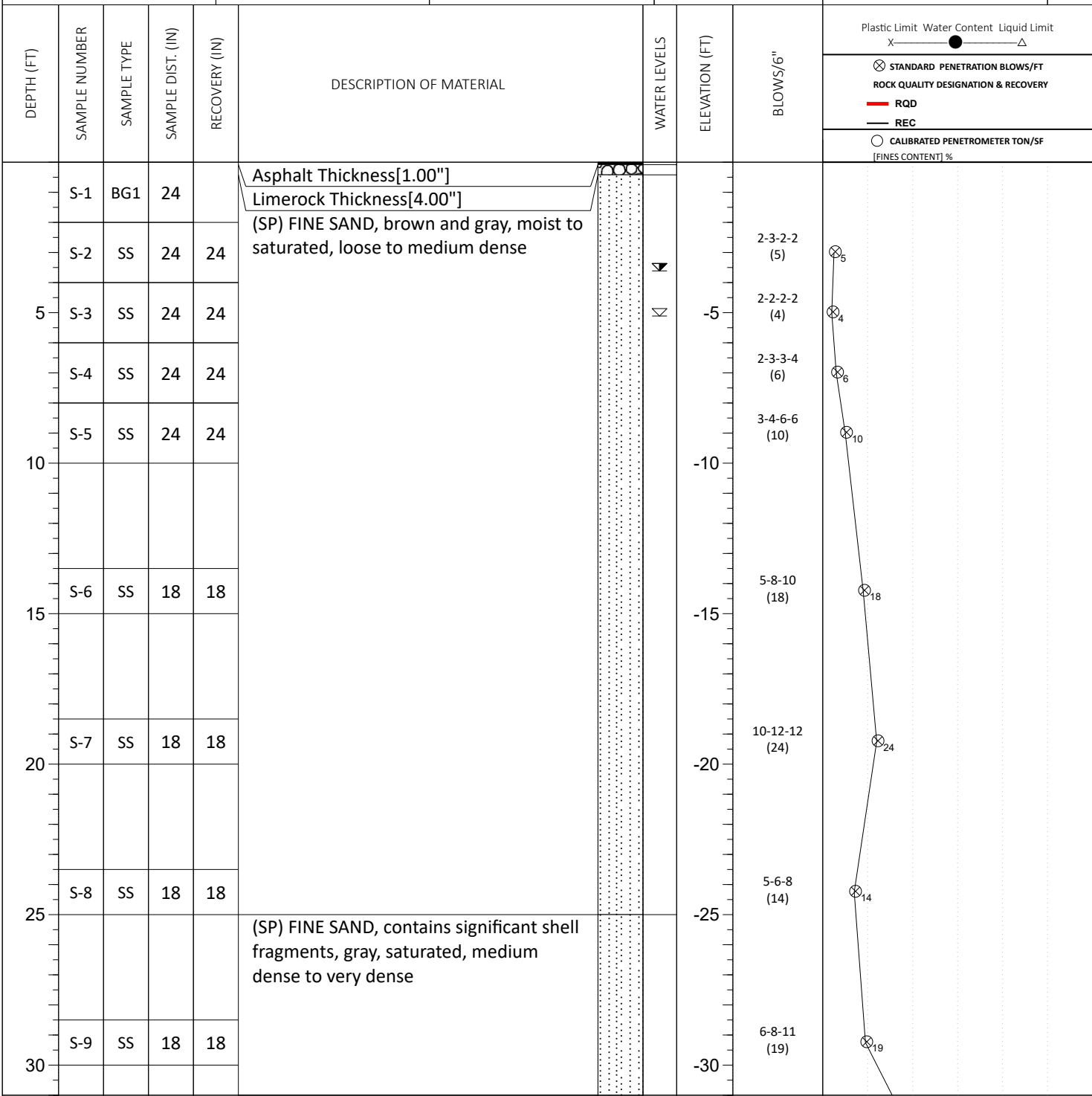
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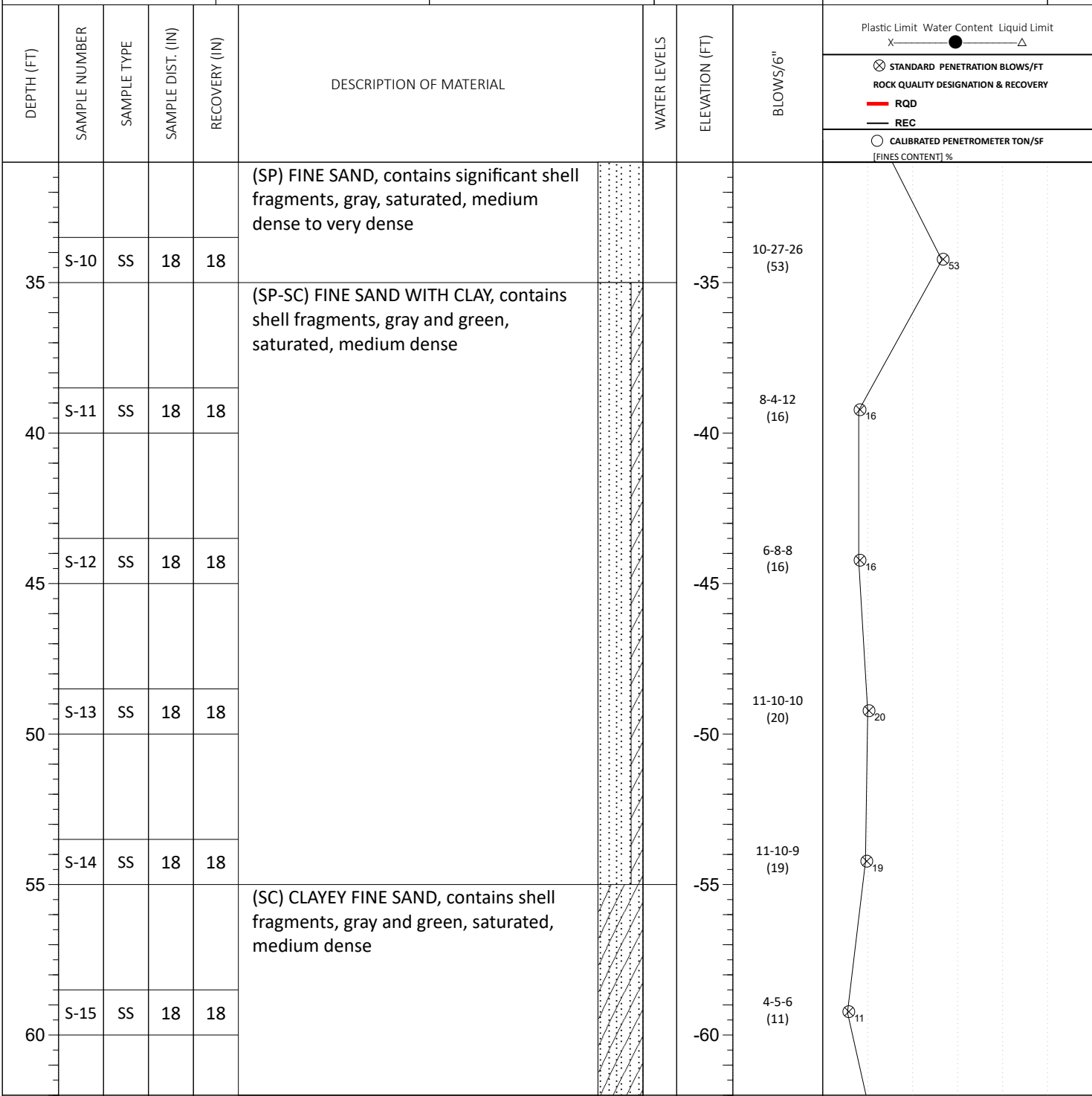
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SITE LOCATION: <b>3550 S Washington Avenue, Titusville, Florida 32780</b>			LOSS OF CIRCULATION 
NORTHING:	EASTING:	STATION:	BOTTOM OF CASING 



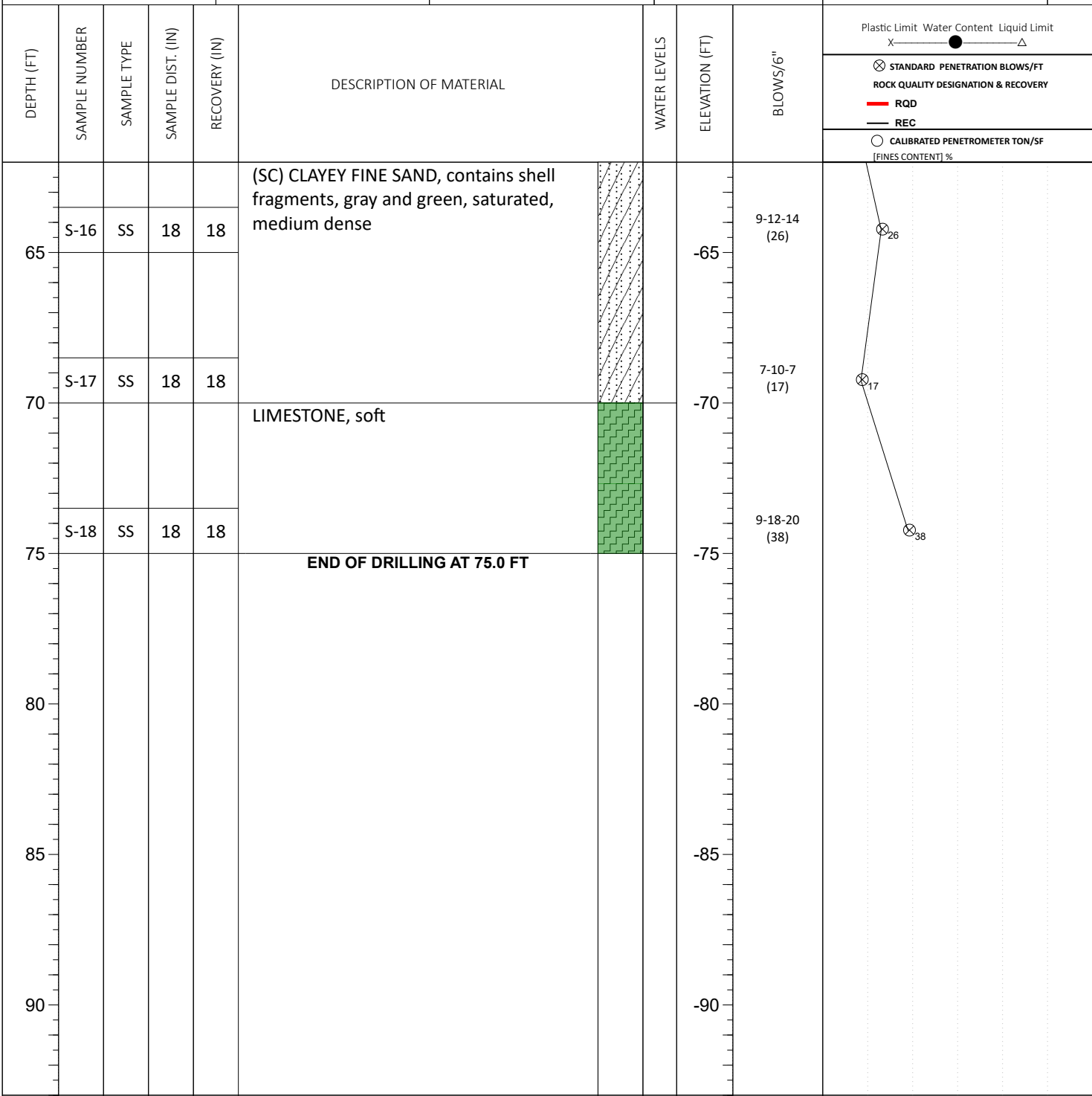
**CONTINUED ON NEXT PAGE**

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

∇ WL (First Encountered) <span style="float: right;"><b>5.00</b></span>	BORING STARTED: <b>Nov 29 2021</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Nov 29 2021</b>	HAMMER TYPE: <b>Manual</b>
∇ WL (Seasonal High Water) <span style="float: right;"><b>3.50</b></span>	EQUIPMENT: <b>Track</b>	DRILLING METHOD: <b>Mud-Rotary</b>
∇ WL (Stabilized)	LOGGED BY: <b>VA1</b>	

**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION: <b>3550 S Washington Avenue, Titusville, Florida 32780</b>				LOSS OF CIRCULATION 
NORTHING:	EASTING:	STATION:	SURFACE ELEVATION:	BOTTOM OF CASING 

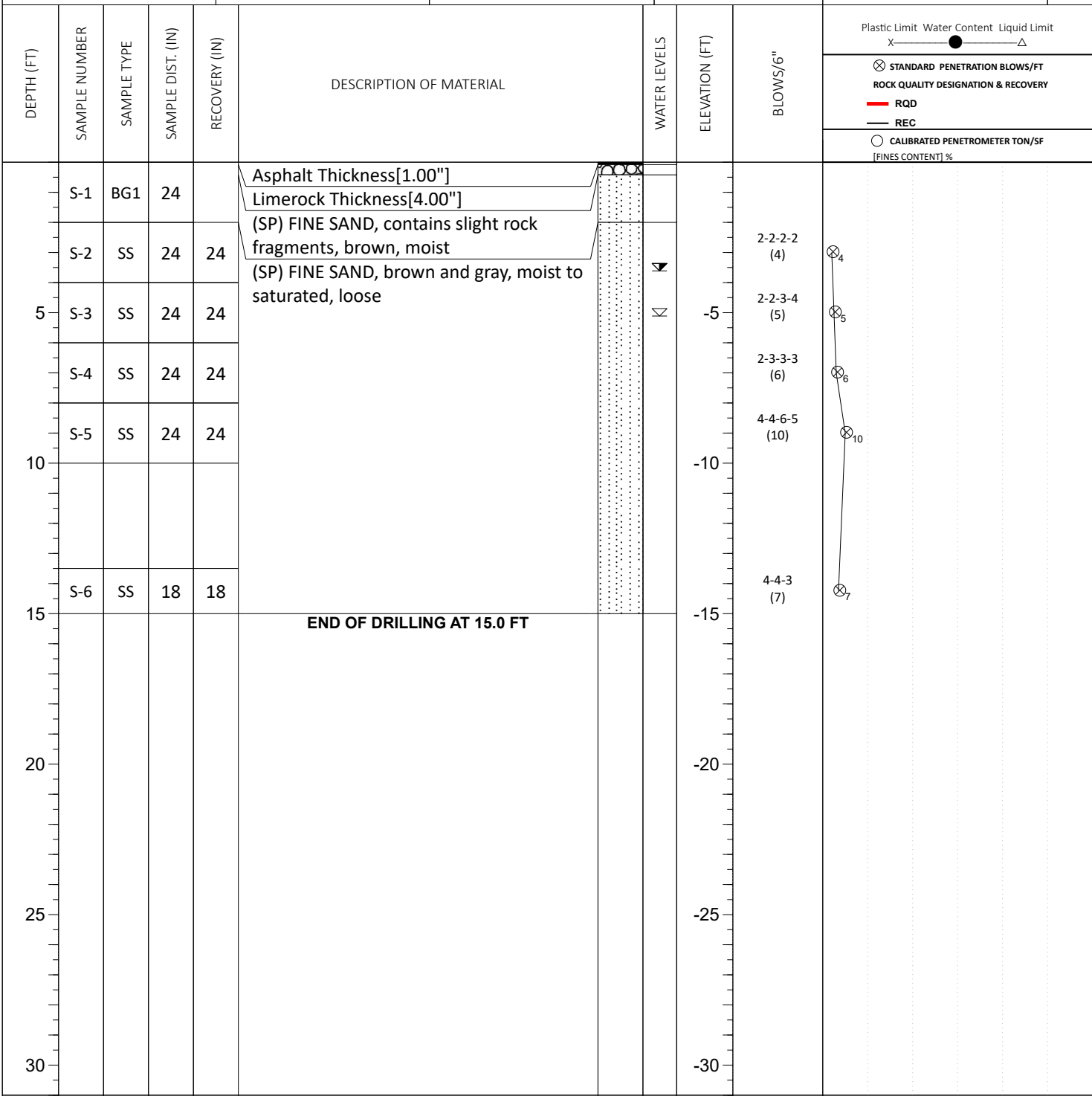


THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

<input checked="" type="checkbox"/> WL (First Encountered) <span style="float: right;"><b>5.00</b></span>	BORING STARTED: <b>Nov 29 2021</b>	CAVE IN DEPTH:
<input checked="" type="checkbox"/> WL (Completion)	BORING COMPLETED: <b>Nov 29 2021</b>	HAMMER TYPE: <b>Manual</b>
<input checked="" type="checkbox"/> WL (Seasonal High Water) <span style="float: right;"><b>3.50</b></span>	EQUIPMENT: <b>Track</b>	LOGGED BY: <b>VA1</b>
<input checked="" type="checkbox"/> WL (Stabilized)		DRILLING METHOD: <b>Mud-Rotary</b>

**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION: <b>3550 S Washington Avenue, Titusville, Florida 32780</b>			LOSS OF CIRCULATION 
NORTHING:	EASTING:	STATION:	BOTTOM OF CASING 



Plastic Limit Water Content Liquid Limit  
 X ● ———— Δ

⊗ STANDARD PENETRATION BLOWS/FT  
 ROCK QUALITY DESIGNATION & RECOVERY

— RQD  
 — REC

○ CALIBRATED PENETROMETER TON/SF  
 [FINES CONTENT] %

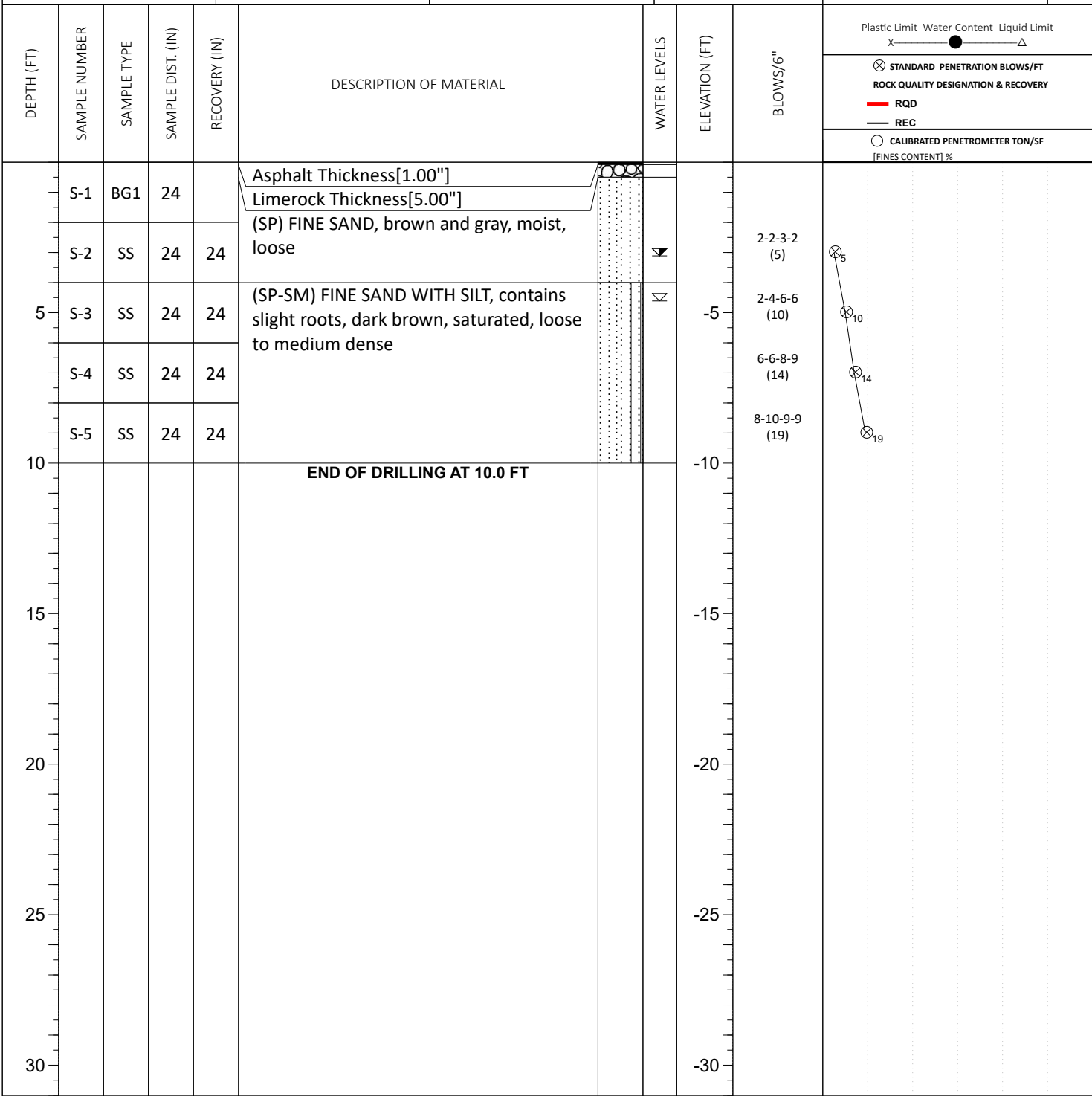
THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

∇ WL (First Encountered) <span style="float: right;"><b>5.00</b></span>	BORING STARTED: <b>Nov 29 2021</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Dec 02 2021</b>	HAMMER TYPE: <b>Manual</b>
∇ WL (Seasonal High Water) <span style="float: right;"><b>3.50</b></span>	EQUIPMENT: <b>Track</b>	DRILLING METHOD: <b>Mud-Rotary</b>
∇ WL (Stabilized)	LOGGED BY: <b>VA1</b>	

**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION:  
**3550 S Washington Avenue, Titusville, Florida 32780**


NORTHING:	EASTING:	STATION:	SURFACE ELEVATION:	LOSS OF CIRCULATION
				BOTTOM OF CASING



THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

▽ WL (First Encountered) <span style="float: right;"><b>4.50</b></span>	BORING STARTED: <b>Dec 01 2021</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Dec 01 2021</b>	HAMMER TYPE: <b>Manual</b>
▽ WL (Seasonal High Water) <span style="float: right;"><b>3.00</b></span>	EQUIPMENT: <b>Track</b>	LOGGED BY: <b>VA1</b>
▽ WL (Stabilized)		DRILLING METHOD: <b>Mud-Rotary</b>

**GEOTECHNICAL BOREHOLE LOG**

CLIENT: <b>California Retail Properties Corp.</b>	PROJECT NO.: <b>56:1380-A</b>	SHEET: <b>1 of 1</b>	
PROJECT NAME: <b>Titusville Resort &amp; Destination</b>	HAND AUGER NO.: <b>R-01</b>	SURFACE ELEVATION:	
SITE LOCATION: <b>3550 S Washington Avenue, Titusville, Florida 32780</b>		STATION:	
NORTHING:	EASTING:		


DEPTH (FT)	WATER LEVELS	ELEVATION (FT)	DESCRIPTION OF MATERIAL	EXCAVATION EFFORT	DCP	SAMPLE NUMBER	FINES CONTENT (%)	MOISTURE CONTENT (%)
5	▼	-5	Asphalt Thickness[1.50"]	E		S-1		
			Limerock Thickness[6.00"]					
			(SP) FINE SAND, brown and gray, moist to saturated					
				E		S-2		
				E		S-3		
10		-10	<b>END OF DRILLING AT 6.0 FT</b>					
15								

REMARKS:

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDRY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL  
EXCAVATION EFFORT: E - EASY M - MEDIUM D - DIFFICULT VD - VERY DIFFICULT

▽ WL (First Encountered) <b>4.50</b>	▼ WL (Seasonal High) <b>3.00</b>	ECS REP:	DATE COMPLETED:	UNITS:	CAVE-IN-DEPTH:
▼ WL (Completion)			<b>Dec 01 2021</b>	<b>English</b>	

**HAND AUGER LOG**

CLIENT: <b>California Retail Properties Corp.</b>	PROJECT NO.: <b>56:1380-A</b>	SHEET: <b>1 of 1</b>	
PROJECT NAME: <b>Titusville Resort &amp; Destination</b>	HAND AUGER NO.: <b>R-02</b>	SURFACE ELEVATION:	
SITE LOCATION: <b>3550 S Washington Avenue, Titusville, Florida 32780</b>		STATION:	
NORTHING:	EASTING:		


DEPTH (FT)	WATER LEVELS	ELEVATION (FT)	DESCRIPTION OF MATERIAL	EXCAVATION EFFORT	DCP	SAMPLE NUMBER	FINES CONTENT (%)	MOISTURE CONTENT (%)
5	▽	-5	Asphalt Thickness[1.50"]	E		S-1		
			Limerock Thickness[4.00"]					
			(SP) FINE SAND, brown and gray, moist to saturated					
				E		S-2		
				E		S-3		
			<b>END OF DRILLING AT 6.0 FT</b>					
10		-10						
15								

REMARKS:

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDRY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL  
EXCAVATION EFFORT: E - EASY M - MEDIUM D - DIFFICULT VD - VERY DIFFICULT

▽ WL (First Encountered) <b>5.00</b>	▽ WL (Seasonal High) <b>3.50</b>	ECS REP:	DATE COMPLETED:	UNITS:	CAVE-IN-DEPTH:
▼ WL (Completion)			<b>Dec 02 2021</b>	<b>English</b>	

**HAND AUGER LOG**

CLIENT: <b>California Retail Properties Corp.</b>	PROJECT NO.: <b>56:1380-A</b>	SHEET: <b>1 of 1</b>	
PROJECT NAME: <b>Titusville Resort &amp; Destination</b>	HAND AUGER NO.: <b>R-03</b>	SURFACE ELEVATION:	
SITE LOCATION: <b>3550 S Washington Avenue, Titusville, Florida 32780</b>		STATION:	
NORTHING:	EASTING:		


DEPTH (FT)	WATER LEVELS	ELEVATION (FT)	DESCRIPTION OF MATERIAL	EXCAVATION EFFORT	DCP	SAMPLE NUMBER	FINES CONTENT (%)	MOISTURE CONTENT (%)
5	▽	-5	Asphalt Thickness[1.50"]	E		S-1		
			Limerock Thickness[6.00"]					
			(SP) FINE SAND, brown and gray, moist to saturated					
				E		S-2		
				E		S-3		
			<b>END OF DRILLING AT 6.0 FT</b>					
10		-10						
15								

REMARKS:

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDRY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL  
EXCAVATION EFFORT: E - EASY M - MEDIUM D - DIFFICULT VD - VERY DIFFICULT

▽ WL (First Encountered) <b>5.00</b>	▽ WL (Seasonal High) <b>3.50</b>	ECS REP:	DATE COMPLETED:	UNITS:	CAVE-IN-DEPTH:
▼ WL (Completion)			<b>Dec 02 2021</b>	<b>English</b>	

**HAND AUGER LOG**

CLIENT: <b>California Retail Properties Corp.</b>	PROJECT NO.: <b>56:1380-A</b>	SHEET: <b>1 of 1</b>	
PROJECT NAME: <b>Titusville Resort &amp; Destination</b>	HAND AUGER NO.: <b>R-04</b>	SURFACE ELEVATION:	
SITE LOCATION: <b>3550 S Washington Avenue, Titusville, Florida 32780</b>		STATION:	
NORTHING:	EASTING:		


DEPTH (FT)	WATER LEVELS	ELEVATION (FT)	DESCRIPTION OF MATERIAL	EXCAVATION EFFORT	DCP	SAMPLE NUMBER	FINES CONTENT (%)	MOISTURE CONTENT (%)
5	▽	-5	Asphalt Thickness[1.00"]	E		S-1		
			Limerock Thickness[5.00"]			S-2		
			(SP) FINE SAND, brown and gray, moist to saturated					
			END OF DRILLING AT 6.0 FT	E		S-3		
10		-10						
15								

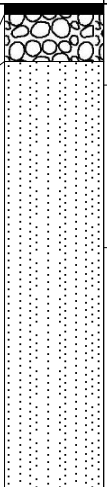
REMARKS:

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDRY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL  
EXCAVATION EFFORT: E - EASY M - MEDIUM D - DIFFICULT VD - VERY DIFFICULT

▽ WL (First Encountered) <b>5.00</b>	▽ WL (Seasonal High) <b>3.50</b>	ECS REP:	DATE COMPLETED:	UNITS:	CAVE-IN-DEPTH:
▼ WL (Completion)			<b>Dec 02 2021</b>	<b>English</b>	

**HAND AUGER LOG**

CLIENT: <b>California Retail Properties Corp.</b>	PROJECT NO.: <b>56:1380-A</b>	SHEET: <b>1 of 1</b>	
PROJECT NAME: <b>Titusville Resort &amp; Destination</b>	HAND AUGER NO.: <b>R-05</b>	SURFACE ELEVATION:	
SITE LOCATION: <b>3550 S Washington Avenue, Titusville, Florida 32780</b>		STATION:	
NORTHING:	EASTING:		


DEPTH (FT)	WATER LEVELS	ELEVATION (FT)	DESCRIPTION OF MATERIAL	EXCAVATION EFFORT	DCP	SAMPLE NUMBER	FINES CONTENT (%)	MOISTURE CONTENT (%)
5	▼	-5	Asphalt Thickness[1.50"]		E	S-1		
			Limerock Thickness[7.00"]			S-2		
			(SP) FINE SAND, brown and gray, moist to saturated			S-3		
10		-10	<b>END OF DRILLING AT 6.0 FT</b>					
15								

REMARKS:

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDRY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL  
EXCAVATION EFFORT: E - EASY M - MEDIUM D - DIFFICULT VD - VERY DIFFICULT

▽ WL (First Encountered) <b>4.50</b>	▼ WL (Seasonal High) <b>3.00</b>	ECS REP:	DATE COMPLETED:	UNITS:	CAVE-IN-DEPTH:
▼ WL (Completion)			<b>Dec 02 2021</b>	<b>English</b>	

**HAND AUGER LOG**

CLIENT: <b>California Retail Properties Corp.</b>	PROJECT NO.: <b>56:1380-A</b>	SHEET: <b>1 of 1</b>	
PROJECT NAME: <b>Titusville Resort &amp; Destination</b>	HAND AUGER NO.: <b>R-06</b>	SURFACE ELEVATION:	
SITE LOCATION: <b>3550 S Washington Avenue, Titusville, Florida 32780</b>		STATION:	
NORTHING:	EASTING:		


DEPTH (FT)	WATER LEVELS	ELEVATION (FT)	DESCRIPTION OF MATERIAL	EXCAVATION EFFORT	DCP	SAMPLE NUMBER	FINES CONTENT (%)	MOISTURE CONTENT (%)
5	▽	-5	Asphalt Thickness[1.00"]	E		S-1		
			Limerock Thickness[4.00"]			S-2		
			(SP) FINE SAND, brown and gray, moist to saturated			S-3		
15			<b>END OF DRILLING AT 6.0 FT</b>					

REMARKS:

THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDRY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL  
EXCAVATION EFFORT: E - EASY M - MEDIUM D - DIFFICULT VD - VERY DIFFICULT

▽ WL (First Encountered) <b>5.00</b>	▽ WL (Seasonal High) <b>3.50</b>	ECS REP:	DATE COMPLETED:	UNITS:	CAVE-IN-DEPTH:
▼ WL (Completion)			<b>Dec 02 2021</b>	<b>English</b>	

**HAND AUGER LOG**

CLIENT: <b>California Retail Properties Corp.</b>	PROJECT NO.: <b>56:1380-A</b>	SHEET: <b>1 of 1</b>	
PROJECT NAME: <b>Titusville Resort &amp; Destination</b>	HAND AUGER NO.: <b>R-07</b>	SURFACE ELEVATION:	
SITE LOCATION: <b>3550 S Washington Avenue, Titusville, Florida 32780</b>		STATION:	
NORTHING:	EASTING:		

DEPTH (FT)	WATER LEVELS	ELEVATION (FT)	DESCRIPTION OF MATERIAL	EXCAVATION EFFORT	DCP	SAMPLE NUMBER	FINES CONTENT (%)	MOISTURE CONTENT (%)
5	▼	-5	Asphalt Thickness[1.00"]	E		S-1		
			Limerock Thickness[6.00"]			S-2		
			(SP) FINE SAND, brown and gray, moist to saturated					
			END OF DRILLING AT 6.0 FT	E		S-3		
10		-10						
15								

REMARKS:

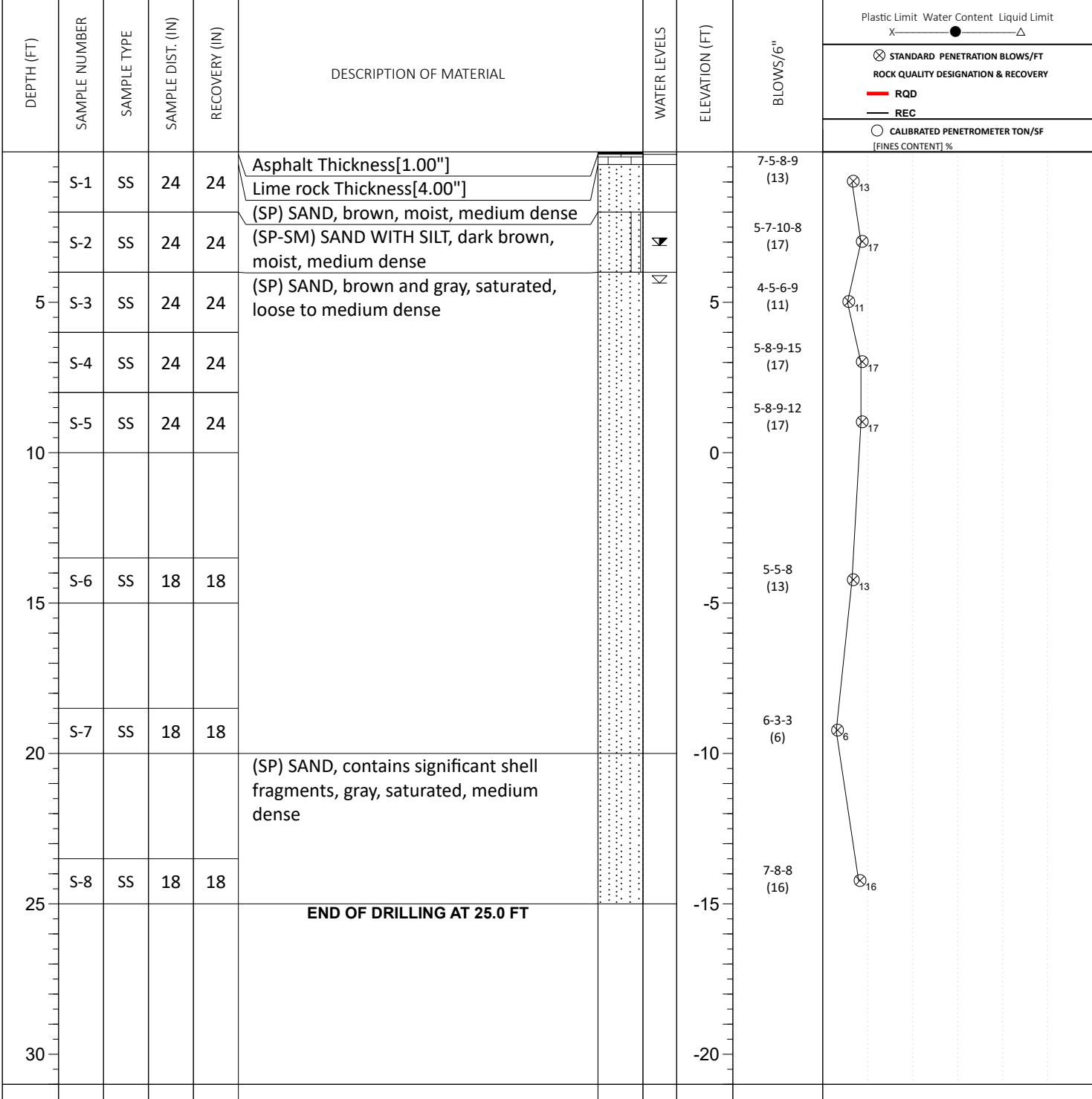
THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDRY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL  
EXCAVATION EFFORT: E - EASY M - MEDIUM D - DIFFICULT VD - VERY DIFFICULT

▽ WL (First Encountered) <b>4.50</b>	▼ WL (Seasonal High) <b>3.00</b>	ECS REP:	DATE COMPLETED:	UNITS:	CAVE-IN-DEPTH:
▼ WL (Completion)			<b>Dec 02 2021</b>	<b>English</b>	

**HAND AUGER LOG**

SITE LOCATION:  
**3550 S. Washington Avenue, Titusville, Florida 32780**

NORTHING: <b>1542235.7</b>	EASTING: <b>720101.6</b>	STATION:	SURFACE ELEVATION: <b>10.0</b>	LOSS OF CIRCULATION
				BOTTOM OF CASING



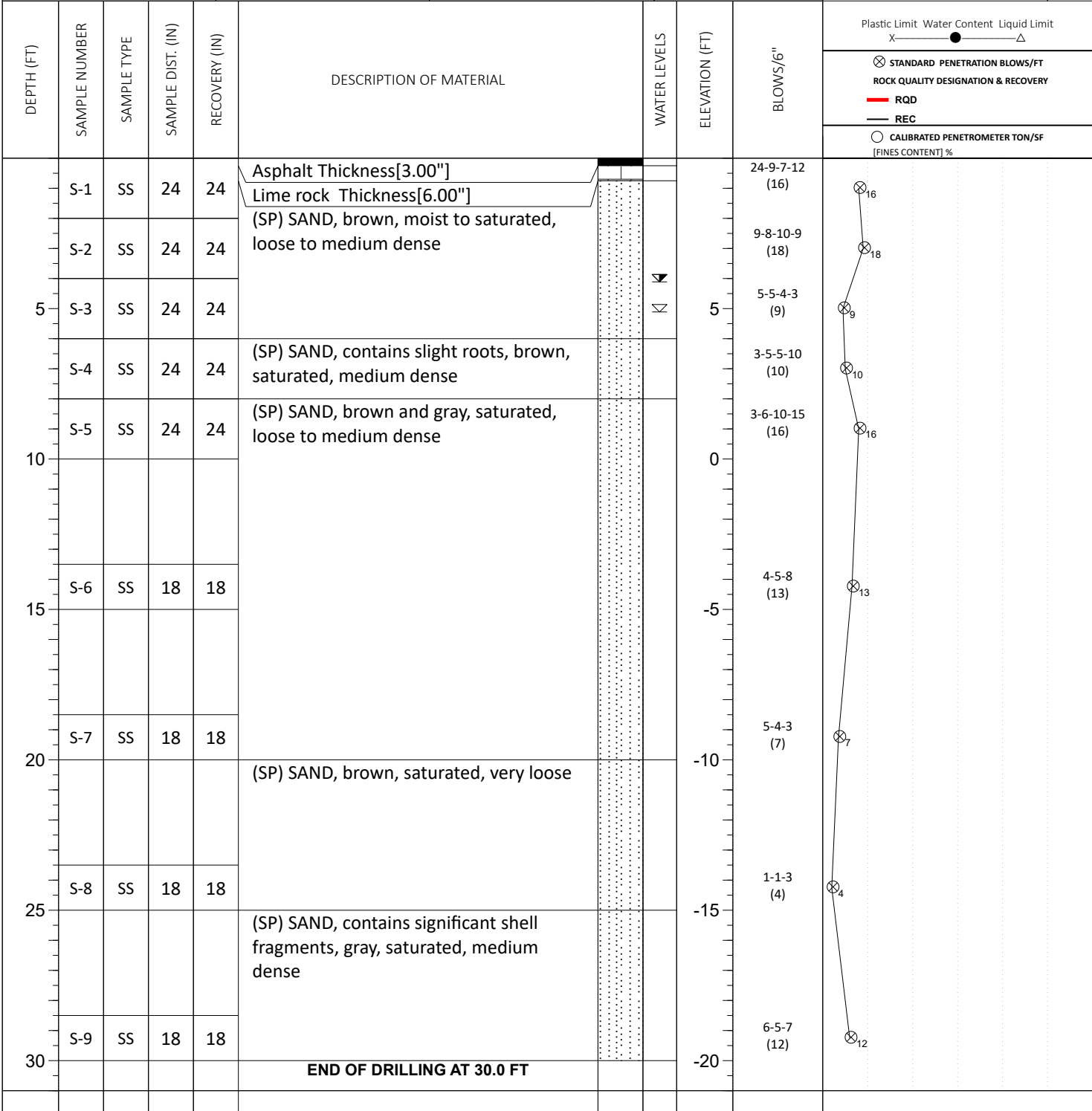
THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

WL (First Encountered) <b>4.25</b>	BORING STARTED: <b>Mar 05 2021</b>	CAVE IN DEPTH:
WL (Completion)	BORING COMPLETED: <b>Mar 05 2021</b>	HAMMER TYPE: <b>Auto</b>
WL (Seasonal High Water) <b>3.00</b>	EQUIPMENT: <b>Truck</b>	LOGGED BY:
WL (Stabilized)		DRILLING METHOD: <b>Mud-Rotary</b>

**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION:  
**3550 S. Washington Avenue, Titusville, Florida 32780**

NORTHING: **1542117.9**      EASTING: **719846.9**      STATION:      SURFACE ELEVATION: **10.0**



THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

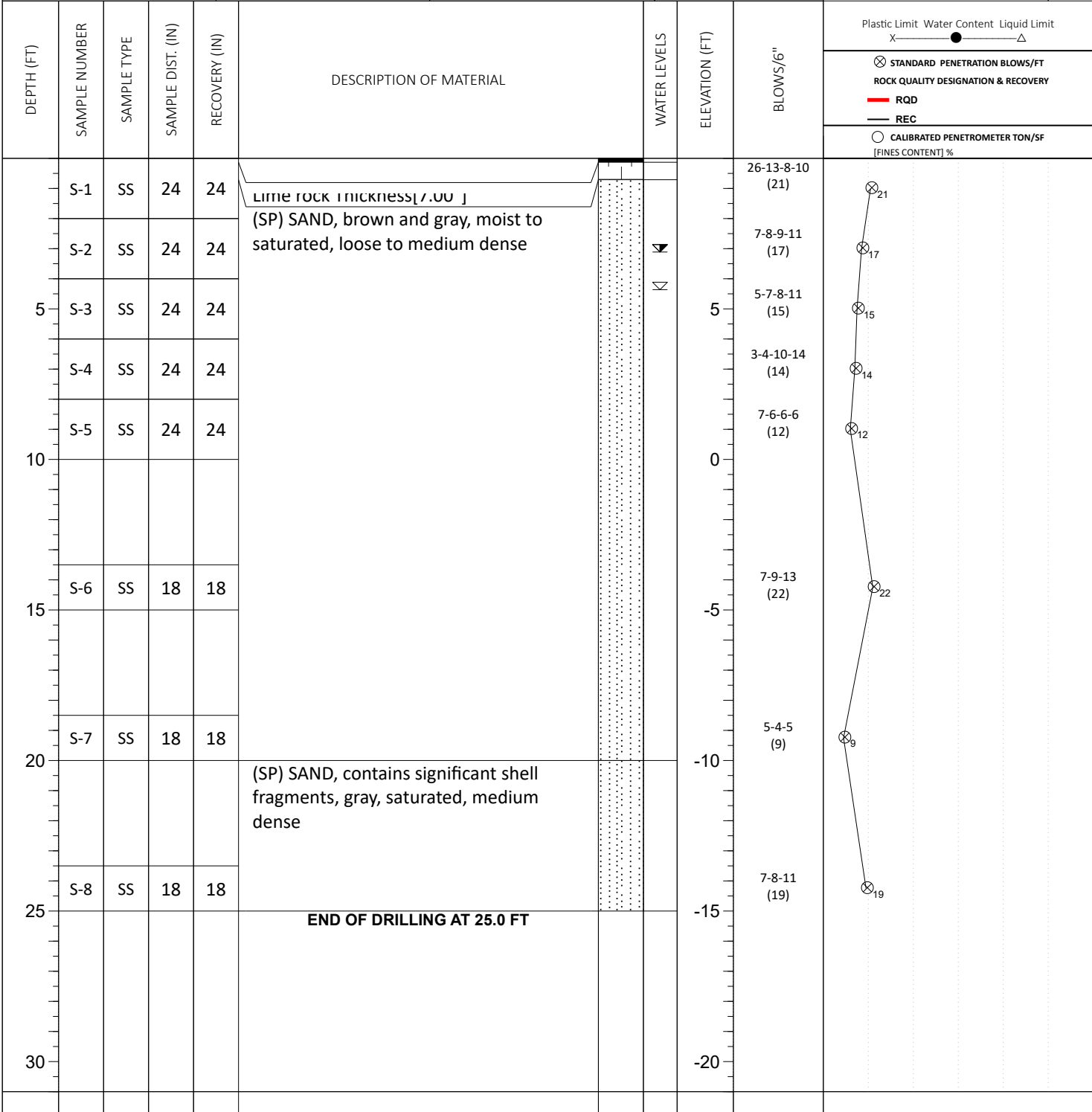
∇ WL (First Encountered) <b>5.00</b>	BORING STARTED: <b>Mar 05 2021</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Mar 05 2021</b>	HAMMER TYPE: <b>Auto</b>
∇ WL (Seasonal High Water) <b>4.00</b>	EQUIPMENT: <b>Truck</b>	LOGGED BY:
∇ WL (Stabilized)		DRILLING METHOD: <b>Mud-Rotary</b>

**GEOTECHNICAL BOREHOLE LOG**



SITE LOCATION:  
**3550 S. Washington Avenue, Titusville, Florida 32780**

NORTHING: **1542296.4**      EASTING: **719509.2**      STATION:      SURFACE ELEVATION: **10.0**



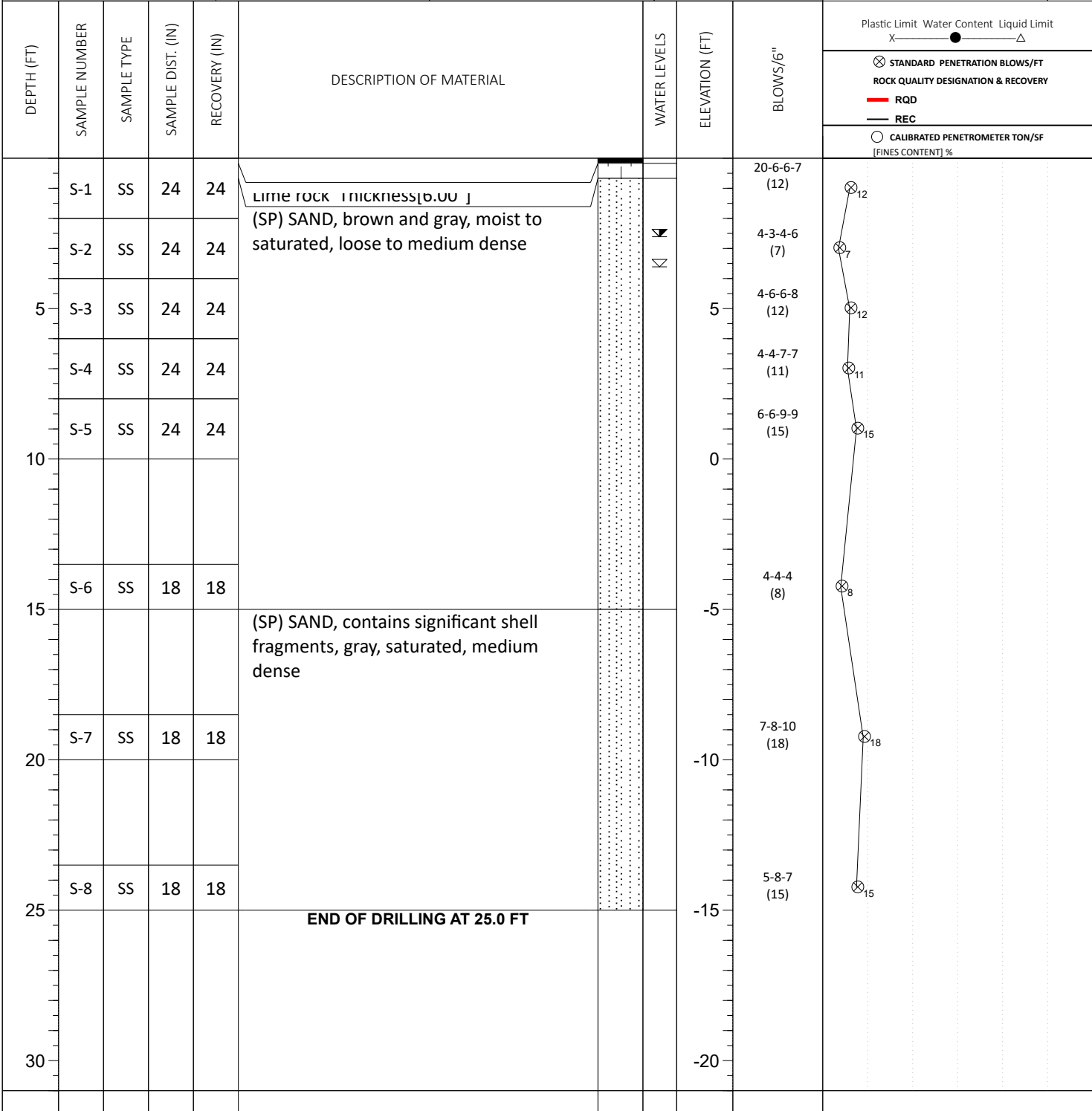
THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

∇ WL (First Encountered) <b>4.25</b>	BORING STARTED: <b>Mar 05 2021</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Mar 05 2021</b>	HAMMER TYPE: <b>Auto</b>
∇ WL (Seasonal High Water) <b>3.00</b>	EQUIPMENT: <b>Truck</b>	LOGGED BY:
∇ WL (Stabilized)		DRILLING METHOD: <b>Mud-Rotary</b>

**GEOTECHNICAL BOREHOLE LOG**

SITE LOCATION:  
**3550 S. Washington Avenue, Titusville, Florida 32780**

NORTHING: **1542018.3**      EASTING: **719172.2**      STATION:      SURFACE ELEVATION: **10.0**



THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

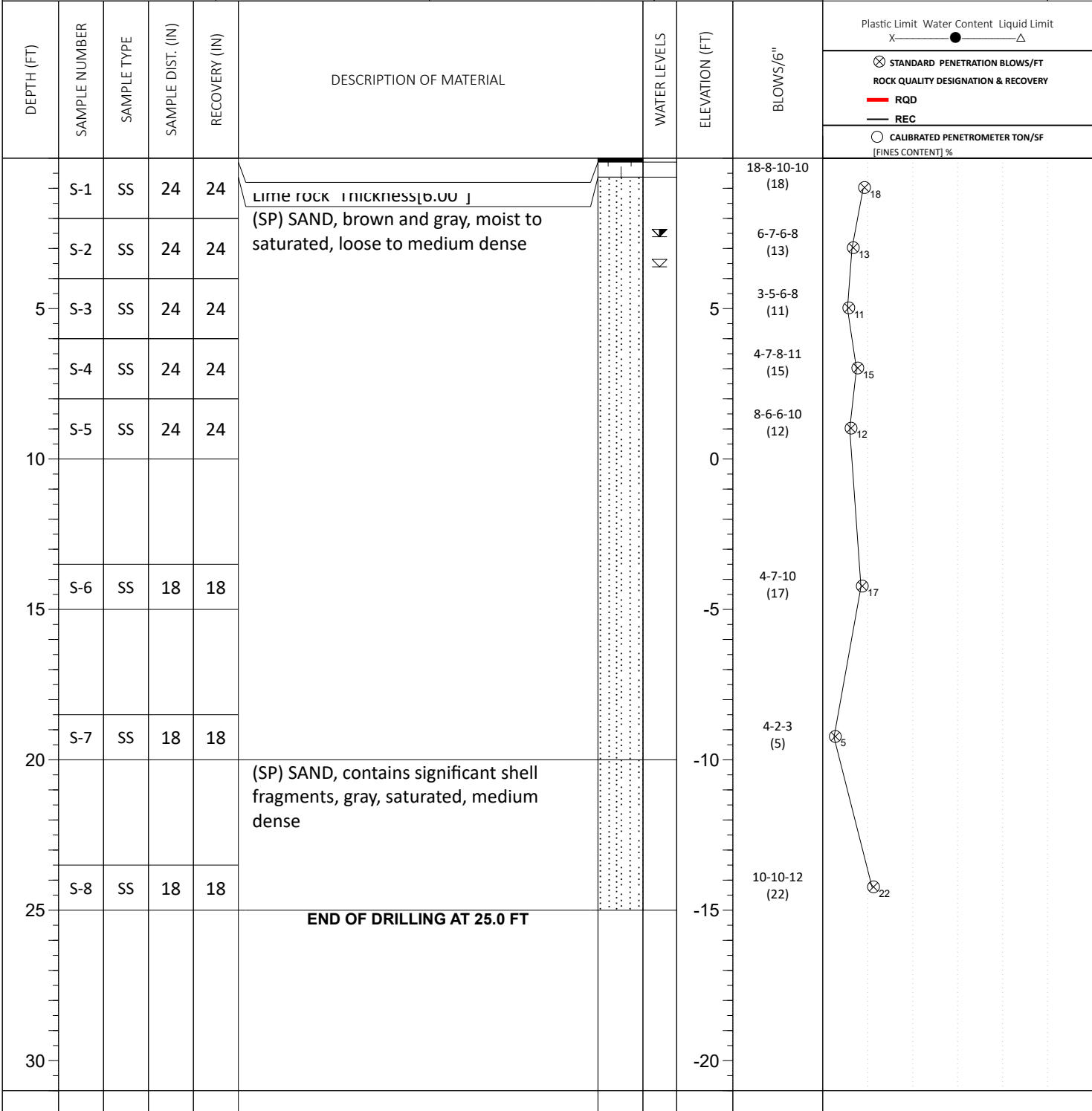
∇ WL (First Encountered) <b>3.50</b>	BORING STARTED: <b>Mar 05 2021</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Mar 05 2021</b>	HAMMER TYPE: <b>Auto</b>
∇ WL (Seasonal High Water) <b>2.50</b>	EQUIPMENT: <b>Truck</b>	LOGGED BY:
∇ WL (Stabilized)		DRILLING METHOD: <b>Mud-Rotary</b>

**GEOTECHNICAL BOREHOLE LOG**



SITE LOCATION:  
**3550 S. Washington Avenue, Titusville, Florida 32780**

NORTHING: **1541761.9**      EASTING: **719455.0**      STATION:      SURFACE ELEVATION: **10.0**



THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

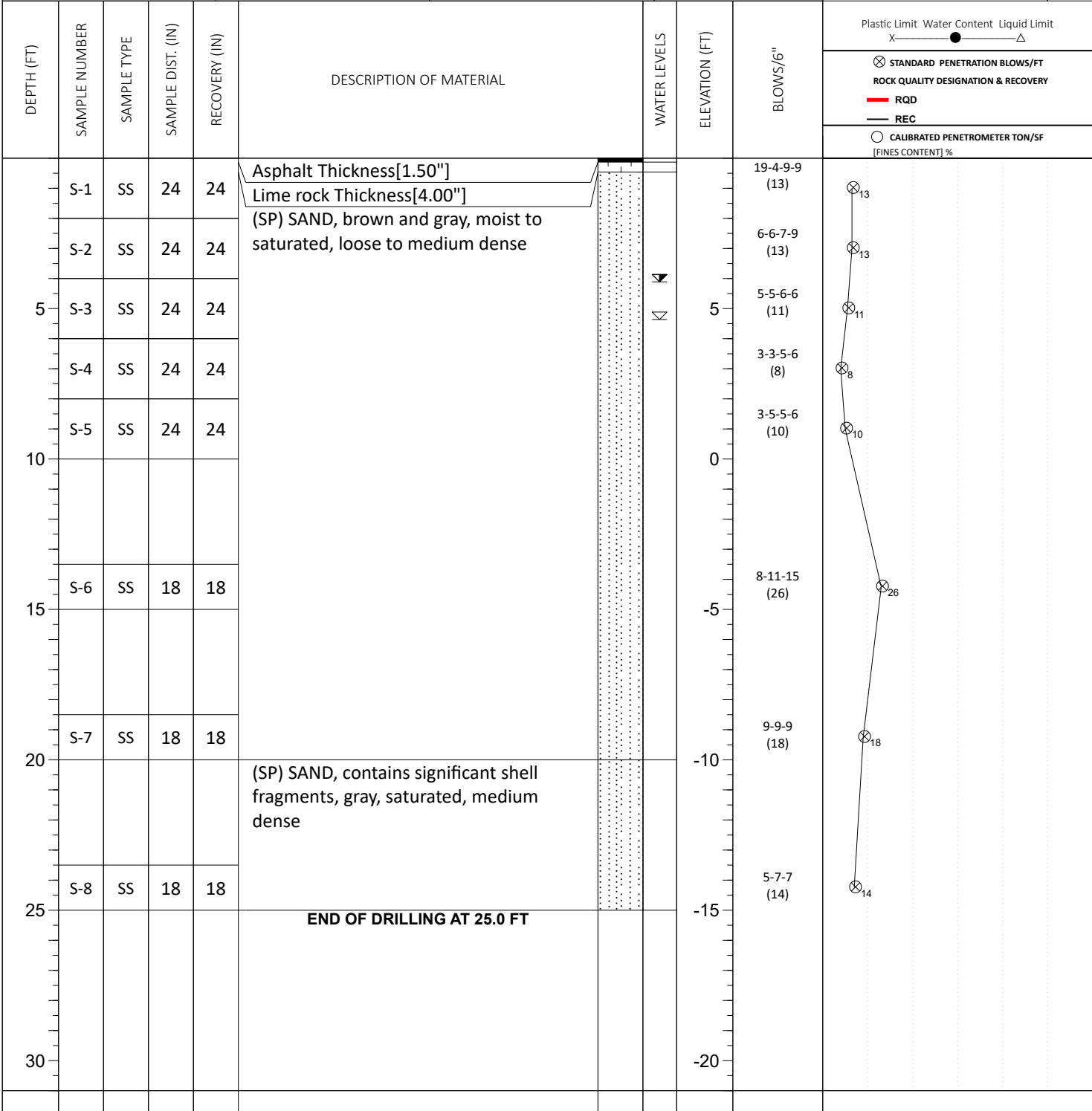
∇ WL (First Encountered) <b>3.50</b>	BORING STARTED: <b>Mar 05 2021</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Mar 05 2021</b>	HAMMER TYPE: <b>Auto</b>
∇ WL (Seasonal High Water) <b>2.50</b>	EQUIPMENT: <b>Truck</b>	LOGGED BY:
∇ WL (Stabilized)		DRILLING METHOD: <b>Mud-Rotary</b>

**GEOTECHNICAL BOREHOLE LOG**



SITE LOCATION:  
**3550 S. Washington Avenue, Titusville, Florida 32780**

NORTHING: **1541855.7**      EASTING: **720257.1**      STATION:      SURFACE ELEVATION: **10.0**



THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES. IN-SITU THE TRANSITION MAY BE GRADUAL

∇ WL (First Encountered) <b>5.25</b>	BORING STARTED: <b>Mar 05 2021</b>	CAVE IN DEPTH:
▼ WL (Completion)	BORING COMPLETED: <b>Mar 05 2021</b>	HAMMER TYPE: <b>Auto</b>
∇ WL (Seasonal High Water) <b>4.00</b>	EQUIPMENT: <b>Truck</b>	LOGGED BY:
∇ WL (Stabilized)		DRILLING METHOD: <b>Mud-Rotary</b>

**GEOTECHNICAL BOREHOLE LOG**

## **APPENDIX C – Laboratory Testing**

Laboratory Test Results Summary



## Laboratory Testing Summary

Sample Location	Sample Number	Depth (feet)	^MC (%)	Soil Type	Atterberg Limits			**Percent Passing No. 200 Sieve	Moisture - Density		@ LBR (%)	#Organic Content (%)
					LL	PL	PI		<Maximum Density (pcf)	<Optimum Moisture (%)		
B-01	S-6	13.5-15	29.7					7.2				
B-02	S-14	53.5-55	27.6					24.9				
B-03	S-11	38.5-40	19.3					4.8				
B-03	S-3	4-6	33.0					20.1				2.4

**Notes:** See test reports for test method, ^ASTM D2216-19, \*ASTM D2488, \*\*ASTM D1140-17, @FM 5-515, #ASTM D2974-20e1 < See test report for D4718 corrected values

**Definitions:** MC: Moisture Content, Soil Type: USCS (Unified Soil Classification System), LL: Liquid Limit, PL: Plastic Limit, PI: Plasticity Index, CBR: California Bearing Ratio, OC: Organic Content

Project: Titusville Mall Redevelopment  
Client: California Retail Properties Corp.

Project No.: 56:1380-B  
Date Reported: 3/27/2024



Office / Lab  
ECS Florida LLC -  
Daytona Beach

Address  
2330 South Nova Road  
Suite A  
South Daytona, FL 32119

Office Number / Fax  
(386)944-9588  
(386)944-9589

Tested by	Checked by	Approved by	Date Received
RRawson	kleimer	kleimer	3/15/2024



## **APPENDIX D – Pressuremeter Test Results**



**Engineering Consulting Services  
Tampa, Florida  
Automated Pressuremeter Summary**

Date: 4/15/2024

Project Number: 56-1380-B

Project Name: Titusville Resort

Project Engineer: TLG

Principal Engineer: DWS

Location	Test	Depth (ft)	Test EL. (ft)	USCS	Pf (tsf)	PI (tsf)	Ep (tsf)	Er	N-SPT	Ep/PI	Ep/N	PI/Pf
PM1	2	11	-1	SP	17.80	9.50	219.00	-	7	23.05	31.29	0.53
PM1	3	24	-14	SP	6.60	4.40	57.96	-	10	13.17	5.80	0.67
PM3	2	14	-4	SP	19.50	13.60	299.57	-	4	22.03	74.89	0.70
PM3	3	29	-19	SP	15.30	10.20	192.64	-	10	18.89	19.26	0.67

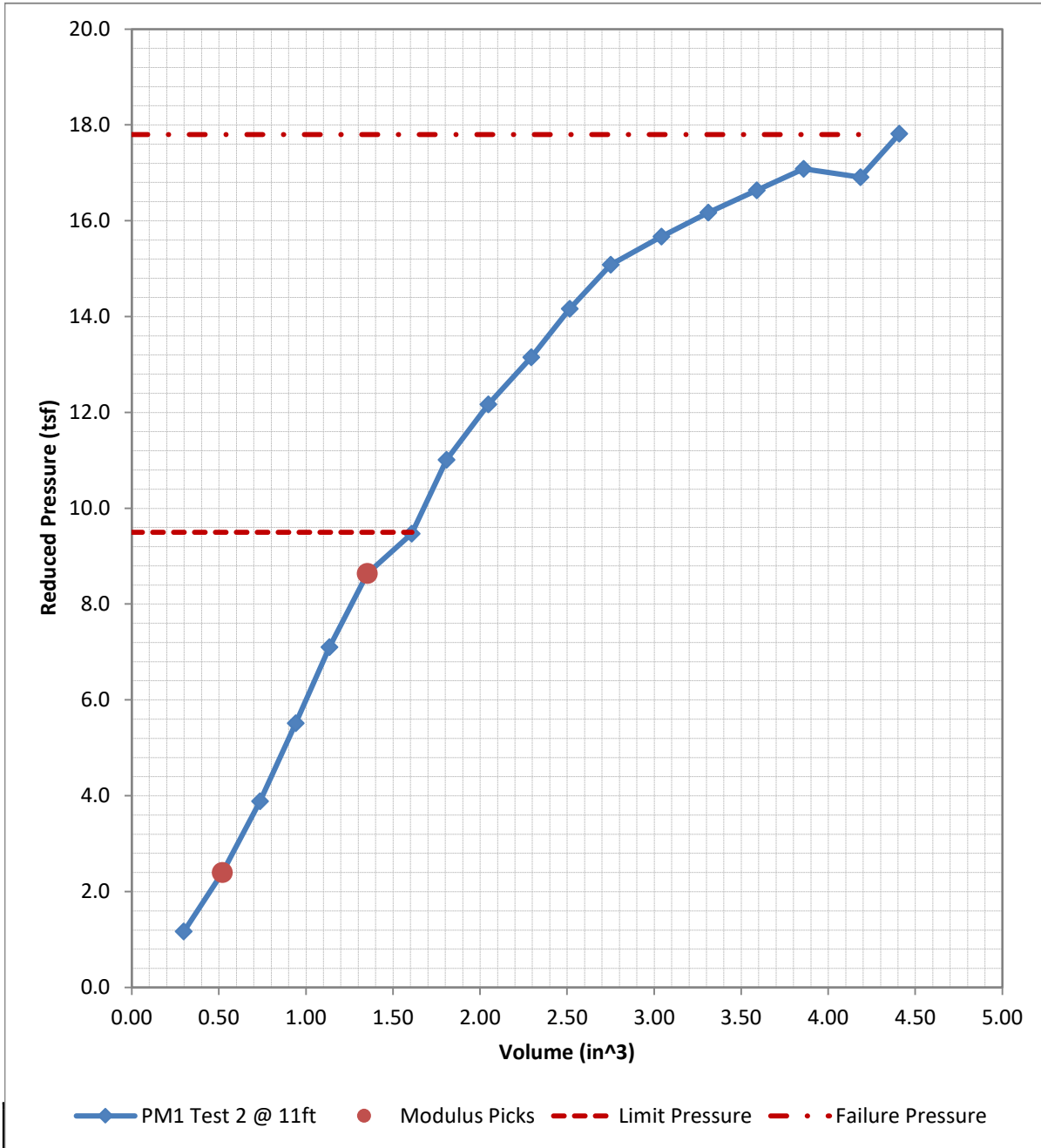
# ECS

## Automated Pressuremeter Report

Membrane Calibration		Volume Calibration	
Pressure (kPa)	Volume (cm <sup>3</sup> )	Pressure (kPa)	Volume (cm <sup>3</sup> )
0.378046	5.189072	1466.43088	59.945402
12.853483	10.016717	1706.866569	62.036521
28.353268	15.283238	1880.388552	63.4306
37.048269	20.188331	2079.995539	65.521719
46.121314	25.196689		
56.706533	30.308313		
63.133273	35.265039		
68.803926	40.247581		
77.120884	45.307571		
80.145232	50.264297		
83.925667	55.091941		
90.730451	60.384279		
92.620669	65.366821		
97.157191	70.29773		
100.559583	75.564251		
102.449801	80.236998		
106.230236	85.271173		
111.900889	90.408612		

# ECS

## Automated Pressuremeter Report



Boring #:	PM1	Test EL (ft):	-1
		Test Depth (ft):	11
Date:	4/15/2024	Project Number:	56-1380-B
Modulus (tsf):	219.00	Limit Pressure (tsf):	9.5
Failure Pressure (tsf):	17.8	N_spt	7
Notes:			

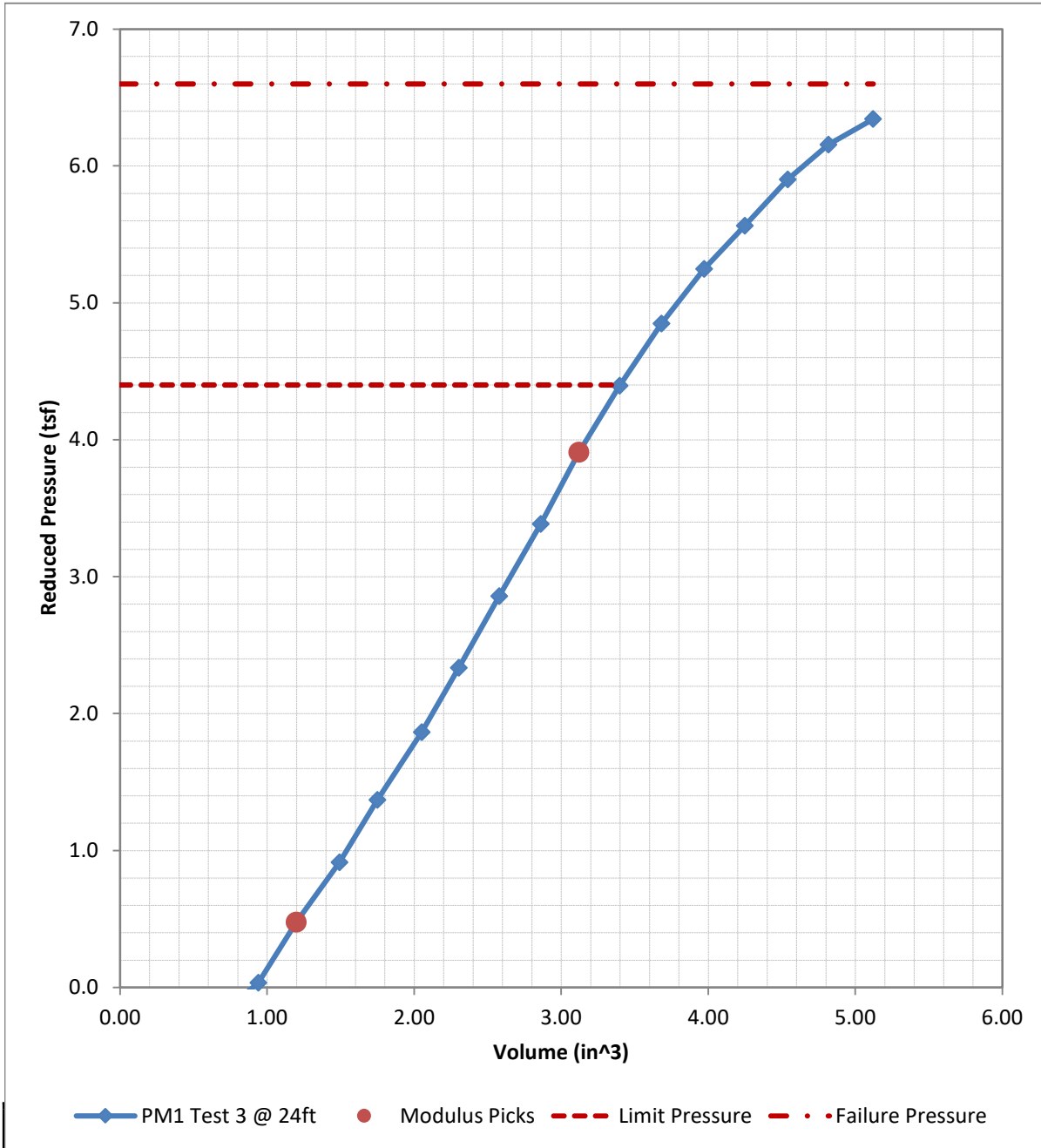
# ECS

## Automated Pressuremeter Report

Pressure (tsf)	Volume (in <sup>3</sup> )		
1.168	0.298		
2.395	0.520		
3.882	0.737	Poisson Ratio	0.333
5.513	0.942	Pressure 1	2.395
7.100	1.135	Pressure 2	8.639
8.639	1.353	Volume 1	0.520
9.468	1.608	Volume 2	1.353
11.007	1.808	E <sub>p</sub> (tsf)	219.001
12.167	2.047	Limit Pressure (tsf)	9.50
13.147	2.294	Failure Pressure (tsf)	17.80
14.160	2.516	N <sub>SPT</sub>	7
15.078	2.751		
15.670	3.042		
16.166	3.311		
16.632	3.590		
17.081	3.858		
16.908	4.186		
17.813	4.408		

# ECS

## Automated Pressuremeter Report



Boring #:	PM1	Test EL (ft):	-14
		Test Depth (ft):	24
Date:	4/15/2024	Project Number:	56-1380-B
Modulus (tsf):	57.96	Limit Pressure (tsf):	4.4
Failure Pressure (tsf):	6.6	N_spt	10
Notes:			

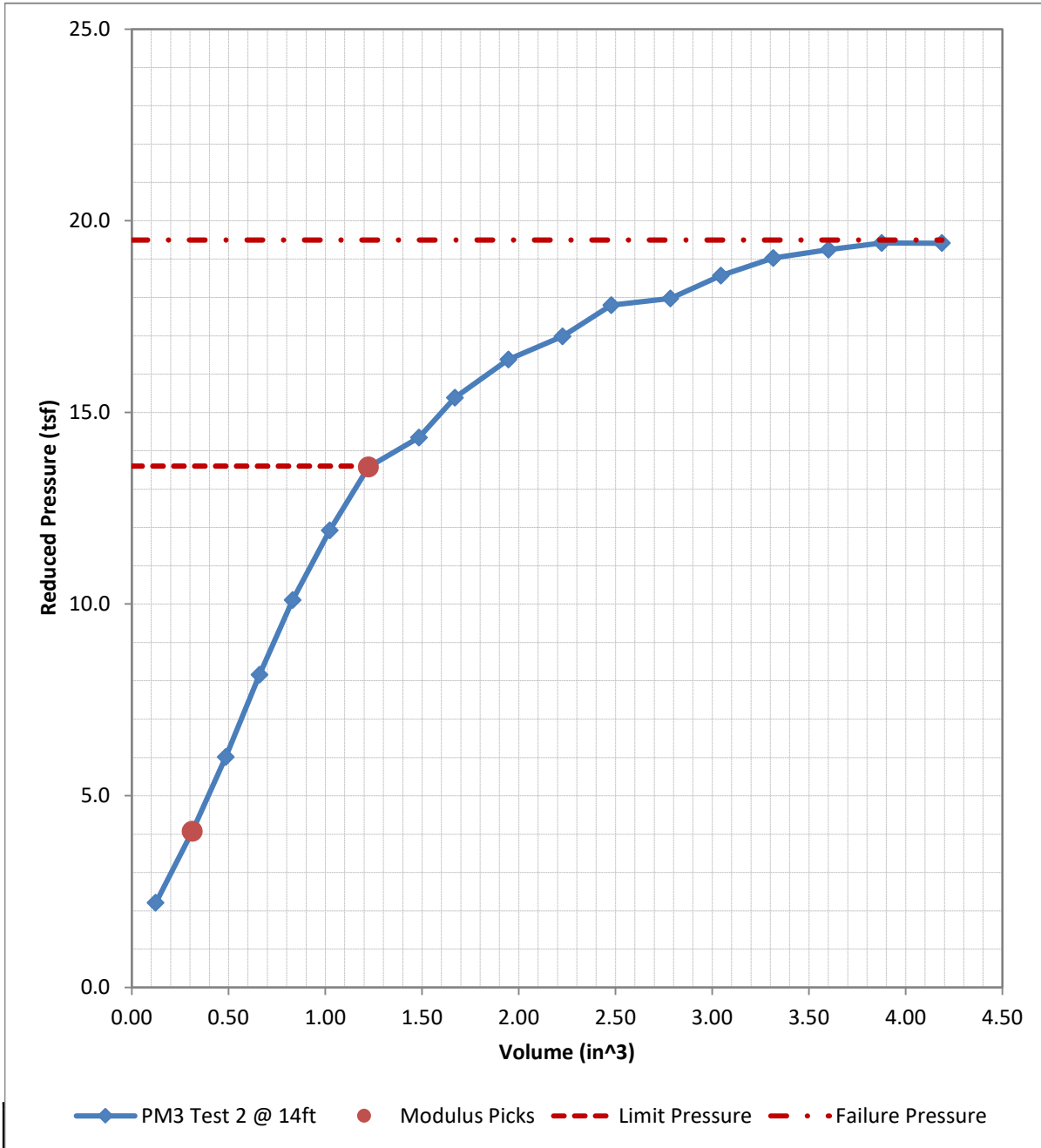
# ECS

## Automated Pressuremeter Report

<u>Pressure (tsf)</u>	<u>Volume (in^3)</u>		
-0.382	0.357		
-0.222	0.664		
0.035	0.940	Poisson Ratio	0.333
0.476	1.199	Pressure 1	0.476
0.914	1.492	Pressure 2	3.909
1.370	1.750	Volume 1	1.199
1.865	2.052	Volume 2	3.122
2.335	2.305	E_p (tsf)	57.955
2.858	2.580	Limit Pressure (tsf)	4.40
3.384	2.862	Failure Pressure (tsf)	6.60
3.909	3.122	N_SPT	10
4.396	3.398		
4.848	3.683		
5.248	3.972		
5.564	4.249		
5.901	4.540		
6.156	4.818		
6.343	5.121		

# ECS

## Automated Pressuremeter Report



PM3 Test 2 @ 14ft		● Modulus Picks		- - - Limit Pressure		- . - . Failure Pressure	
Boring #:	PM3	Test EL (ft):	-4	Test Depth (ft):	14		
Date:	4/15/2024	Project Number:	56-1380-B				
Modulus (tsf):	299.57	Limit Pressure (tsf):	13.6				
Failure Pressure (tsf):	19.5	N_spt	4				
Notes:							

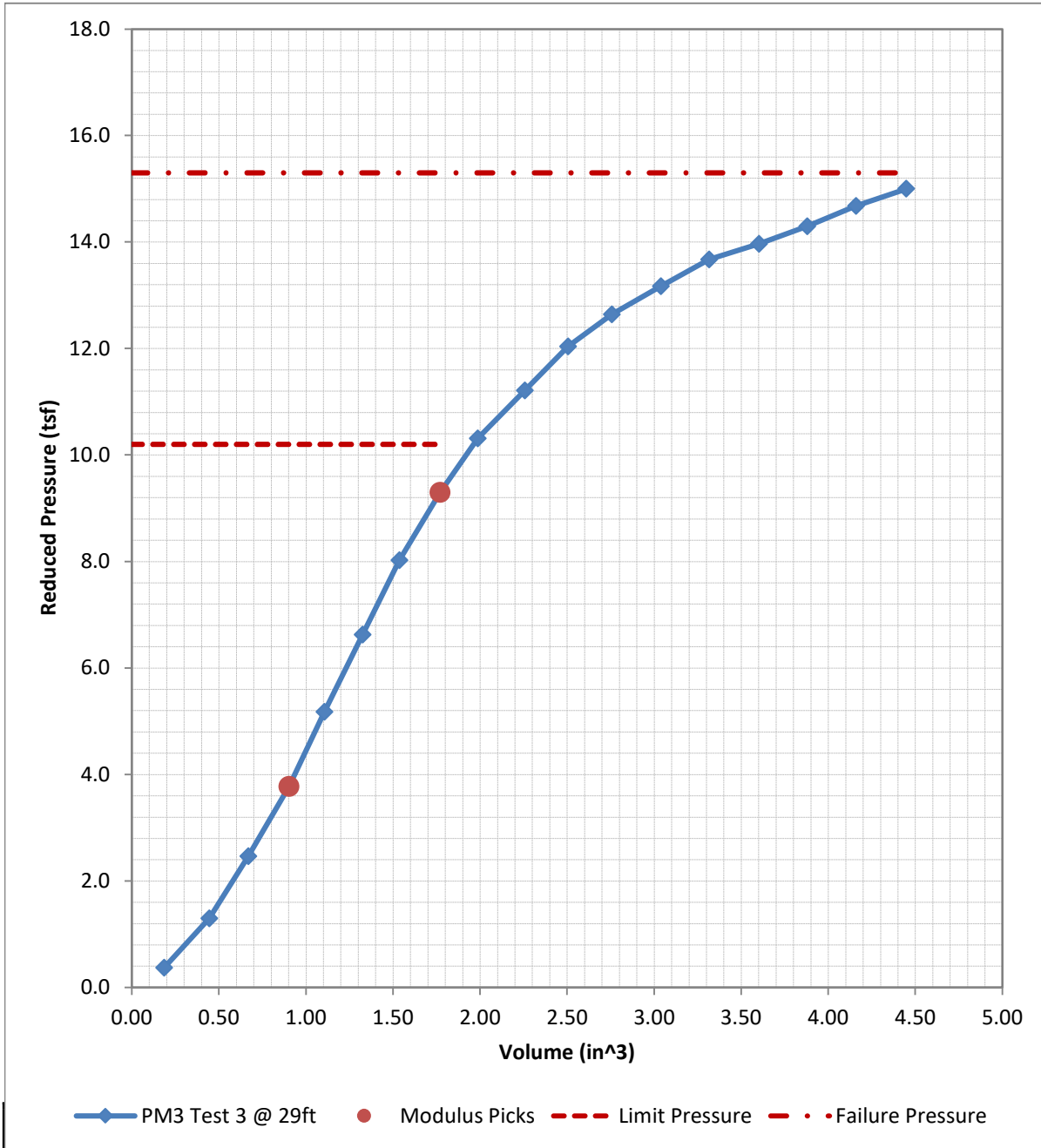
# ECS

## Automated Pressuremeter Report

Pressure (tsf)	Volume (in <sup>3</sup> )		
2.206	0.123		
4.074	0.312		
6.009	0.485	Poisson Ratio	0.333
8.156	0.659	Pressure 1	4.074
10.105	0.832	Pressure 2	13.570
11.921	1.023	Volume 1	0.312
13.570	1.223	Volume 2	1.223
14.341	1.484	E <sub>p</sub> (tsf)	299.575
15.379	1.670	Limit Pressure (tsf)	13.60
16.379	1.947	Failure Pressure (tsf)	19.50
16.986	2.226	N <sub>SPT</sub>	4
17.798	2.478		
17.970	2.784		
18.570	3.045		
19.028	3.316		
19.246	3.601		
19.417	3.876		
19.417	4.188		

# ECS

## Automated Pressuremeter Report



Boring #:	PM3	Test EL (ft):	-19
		Test Depth (ft):	29
Date:	4/15/2024	Project Number:	56-1380-B
Modulus (tsf):	192.64	Limit Pressure (tsf):	10.2
Failure Pressure (tsf):	15.3	N_spt	10
Notes:			

# ECS

## Automated Pressuremeter Report

<u>Pressure (tsf)</u>	<u>Volume (in^3)</u>		
0.371	0.185		
1.297	0.446		
2.463	0.669	Poisson Ratio	0.333
3.772	0.904	Pressure 1	3.772
5.177	1.107	Pressure 2	9.298
6.629	1.326	Volume 1	0.904
8.023	1.537	Volume 2	1.772
9.298	1.772	E_p (tsf)	192.635
10.310	1.987	Limit Pressure (tsf)	10.20
11.210	2.258	Failure Pressure (tsf)	15.30
12.040	2.506	N_SPT	10
12.641	2.757		
13.170	3.039		
13.674	3.316		
13.968	3.603		
14.295	3.879		
14.678	4.159		
14.999	4.448		